TEMPERATURE DEPENDENCE OF THE INTERMOLECULAR ACTIVATION ENERGY FOR FLOW IN LIQUIDS AND SOLUTIONS

Part VII.—Investigation of Steps in the Activation Energy for Some Light Aliphatic Hydrocarbons (C=6 upto C=12)

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Further accurate measurements of activation energy $E\eta$, of viscous flow have been made on several light hydrocarbons, namely n—Hexane, n-Octane, Iso-Octane, n-Decane and Kerosene oil (Molecular weight=165). With the only exception of Iso-Octane, these results show a regular step-wise structure in $E\eta$ at lower temperatures, and cyclic behaviour at fairly high temperatures.

A plot of temperature for this transition versus the number of Carbon atoms, n, gives a smooth curve with the maximum curvature at n=15. An approximately linear graph for $\log(n)$ against this transition temperature has been plotted, together with the freezing and boiling points. These graphs suggest the presence of a transition between two *differently ordered* states of the liquids.

The behaviour of iso-Octane is anamolous in that it shows a cyclic variation at the *lower* temperatures, going over into a constant value of E above the transition temperature.

Introduction

The work done in this laboratory so far, on the precise measurements of activation energy of viscous flow E_{γ} , using small measuring intervals of 1° to 2°C., for different liquids such as water, ethylene glycol and benzene, and solutions like dilute aqueous ethyl alcohol, dilute NaCl, have shown a stepwise behaviour in some cases and cyclic variations in others. In the case of water¹ and dilute ethyl alcohol² definite step-like variations were found, which are a function of temperature and alcohol concentration, while in similar measurements carried out in B.O.C. "60" oil and highspeed diesel oil in the range of 8° to 150°C., reported in part IV of this series,3 steps were observed at the lower temperatures and cyclic behaviour at higher temperatures. The results on light lubricating oil showed a step-like variation having a series of short and long steps with a mean interval of 8°C., and changing over to cyclic variation near a temperature of 136° 73°C. with amplitude of ± 0.1 unit of E/R and mean period of about 12°C. (The temperature of 133°C. reported earlier³ corresponds to the end of the last step, while the first minimum is at 139°C., so that the transition could have occurred anywhere in this range; therefore, it is preferable to quote it as $136^{\circ}C. \mp 3^{\circ}C.$). The high-speed diesel oil ($C_{15}H_{32}$) showed long, clear and sharp steps of similar mag-

nitude, viz. 0.1 unit of E/R, with a very definite constancy over long temperature-ranges, finally going over at 120°C. 72°C. to sinusoidal variations with peak-to-peak amplitude of 0.1 unit of E/R, and period of 12°C. The preliminary data in the range of 10° to 55°C. on n-Decane exhibited only a step-structure, and the jump of 0.08 units of (E/R)/1000 at 20°C. was quite clear. Accordingly, it was considered worthwhile to repeat the measurements on n-Decane to higher temperatures with more precision (by using viscometer No.'O' instead of No. 'I') and to extend the observations to lighter hydrocarbons. The present communication describes these new experiments with improved technique on (1) n-Decane (2) n-Octane, together with its isomer 2:2:4 Trimethyl pentane (3) Hexane, and (4) Kerosene oil (Molecular weight=165).

Experimental Technique

The value of E_{η} is determined as before from the differential of the logarithm of the Andrade equation viz.

$$E/R = \Delta \ln \eta / \Delta (I/T) = -T^2 \Delta \ln \eta / \Delta T$$

which is equivalent to the established procedure of taking the mean slope of the curve for $\ln \eta$ against I/T in the range of T and $T+\Delta T$. The equation (1) can be rearranged as follows:

$$\begin{split} \mathrm{E}_{\gamma}/\mathrm{R} &= -\mathrm{T}^{2}\Delta\mathrm{ln}(\mathrm{v}\times\mathrm{\rho})/\Delta\mathrm{T} \\ &= -\mathrm{T}^{2}\mathrm{ln}\mathrm{v}/\Delta\mathrm{T} + \mathrm{T}^{2}(\frac{1}{\mathrm{\rho}}\,\Delta\mathrm{\rho}/\Delta\mathrm{T}) \\ &= -\mathrm{E}_{\mathrm{v}}/\mathrm{R} + \mathrm{T}^{2}\mathrm{\beta}, \end{split}$$

where η is dynamic viscosity, ν the kinematic viscosity, β the coefficient of dilatation and $T^2\beta$ is a small slowly varying correction term, which is not applied in the actual data given in the tables, but its values are given for some temperatures.

The details of the experimental technique are essentially the same as for the previous experiments on water, long-chain hydrocarbons and aqueous alcohol containing 4 to 14 percent water,4 including vapour equilibrium bottle containing some of the liquid under the test to compensate the evaporation by maintaining dynamic equilibrium. Viscometer No. 'O' (constant being 0.000,735) of British Standard Specification 188, was used, and the flow-times fall between 700 seconds to 1600 seconds, depending upon the temperature and liquid used. When the steady state of temperature had been maintained for nearly 20 minutes, four to six readings were taken for each temperature, and times of flow were measured with a calibrated stop watch graduated to 0.1 seconds, thus giving a reading accuracy of ± 0.02 seconds for each temperature. The actual temperature was read on an ordinary mercury thermometer graduated to 0.1°C., whereas the thermal in-terval ΔT was recorded with a carefully calibrated Beckmann differential thermometer of nearly six degree scale. The height of meniscus of the liquid over the fiducial mark (above the large viscometer bulb) was determined by a cathetometer, giving an estimate to the third place of decimal in mm., and an appropriate correction was applied to the flow times. All these factors ultimately give a reproducibility of ± 0.004 in $E/R \div 1000$, which ranges from 0.8 to 1.2 units for all the different liquids studied here.

Experiments with n-Decane $(C_{10}H_{22})$

The first set of measurements were carried out on n-Decane (BDH, Analar) in the range of 9° to 90°C. with a thermal interval Δ T of 1°C. Viscometer No. 'O' (constant=0.000,735) was used, fixed vertically in a Townson-Mercer Thermostat bath. The actual Beckmann readings and flow times, together with the value of (E/R)/1000 obtained from these during heating and cooling sequences are presented in Table 1, together with the overall means and r.m.s. deviations estimated from the group of five successive observations. These deviations are only 0.004 units as compared with 0.011 in the earlier experiment, and the mean values of (E/R)/1000 are plotted as hollow circles in the lower half of Fig. 1, where the vertical scale is enlarged $2\frac{1}{2}$ times in the previous data shown as solid circles in Fig. 1(top). A comparison shows that, while these two graphs are in essential agreement, the new data provides considerably more detail.

While the old graph (solid circles) only shows jumps at 19-22°C. and 38°C., the new data (hollow circles) shows two steps replacing the previously observed one at 38°C.) and a whole series of regular steps at the average interval of 13°C., each step having a truly horizontal portion, very much like those previously observed with high-speed diesel oil.³ The average depth of the jumps is of the order of 0.04 units of (E/R)/1000, which is ten times the present r.m.s. deviation. This type of step-like variation is seen to continue upto $73^{\circ}C.\mp 2^{\circ}C.$, beyond which the phenomenon undergoes a change, and (E/R)/1000 begins to oscillate with an average peak-to-peak amplitude of 0.06 units and average temperature period of 8°C. This period compares with those previously observed in light lubricating oil (B.O.C. "60") and H.S. diesel, where these variations occur above 133°C. and 118°C., respectively.

Experiments with n-Octane and iso-Octane

Next, the measurements were carried out in the range of 5°C. to 75°C. on n-Octane (C_8H_{18}) , having freezing point of 56.8°C. and boiling point 125.6°C. Extra pure Octane from BDH was transferred to viscometer No. 'O' and flow time was measured to an accuracy of ± 0.02 seconds. Table 2(a) gives the values of (E/R)/1000 obtained during heating and cooling, and the overall mean (E/R)/1000, together with estimated values of r.m.s. deviation for the groups of five successive temperatures, which is seen to be of the order of ± 0.005 units.

Fig. 2(top) is the plot of the overall mean (E/R)/1000 values for n-Octane against temperature, the scale being the same as adopted in the case of n-decane. The curve drawn through the plotted hollow circles shows a clear horizontal straight line extending all the way from 5°C. upto 50°C. with no detectable change in E, which differs from the step-like behaviour observed in other hydrocarbons. However, above $52^{\circ}C. \mp 2^{\circ}C.$, the Energy E begins to oscillate with peak-to-peak amplitude of 0.05 units of (E/R)/1000 and an average cyclic period of 6.2°C.

		Heating sequ	uence					Cooling	sequence			
Tem-	Beck-	Time of	Mean	E/.	R÷1000	Tem-	Beck-	Time of flow	Mean	E/1	R÷1000	Mean
ture °C.	read- ing	ected for level	rature °C.	Uncorr	r- Correc- ted	ture °C.	read- ing	ted for level	rature °C.	Uncorr- ected	Correc- ted	E/R ÷ 1000
 1	2	3	4	5	6	7	8	9	10	11	12	13
9.0	0.183 ± 0.001	377.85±0.01	9.50	1.272	1.275+0.004	9.0	0.189 ± 0.001	377.85±0.01	9.50	1.267	1.271+0.004	1.273 ± 0.002
10.0	1.182 ± 0.000	371.95±0.01	10.50	1.274	1.263 ± 0.004	10.0	1.192 ± 0.000	371.90±0.00	10.50	1.275	1.271 ± 0.004	1.267 ± 0.004
11.0	2.185 ±0.001	300.09±0.02	11.50	1.265	1.271 ± 0.004	11.0	2.189 ± 0.000	366.07 ± 0.01	11.50	1.274	1.280 ± 0.004	1.275±0.005
12.0	3.186 ± 0.000	360.41 ± 0.00 354.87 ± 0.01	12.50	1.271	1.273 ± 0.004	12.0	3.191±0.001	360.35 ± 0.01	12.50	1.266	1.267 ± 0.004	1.270 ± 0.003
13.0	0.008 ± 0.000	354.74 ± 0.00				13.0	0.006 ± 0.001	354.78 ± 0.00 354.78 ± 0.01				
14.0	1.005±0.001	349.31±0.01	13.50	1.272	1.274±0.004	14.0	1.008±0.000	349.32±0.00	13.50	1.272	1.274±0.004	1.274 ± 0.000
15.0	2.007 ± 0.000	343.98±0.00	14.50	1.270	1.273±0.004	15.0	2.003 ± 0.001	344.02±0.02	14.50	1.275	1.279 ± 0.004	1.276±0.003
16.0	3.000 ± 0.001	338.83±0.01	15.50	1,266	1.268 ± 0.004	16.0	3.001±0.000	338.84±0.01	15.50	1.267	1.271 ± 0.004	1.270 ± 0.002
17.0	4.001 ± 0.001	333.73±0.01	17.50	1.271	1.277 ± 0.004	17.0	4.007±0.001	333.71 ± 0.01	17.50	1.272	1.278 ± 0.004	1.278 ± 0.001
18.0	4.999±0.000	328.76 ± 0.00	17.50	1,270	1.203±0.004	18.0	5.000±0.000	328.74 ±-0.01	17.50	1.2//	1.272±0,004	1.200±0.004
18.0	0.110 ± 0.001	328.56 ± 0.02	18.50	1.270	1.273 ± 0.006	18.0	0.119±0.001	328.54 ± 0.01	18.50	1.275	1.278 ± 0.006	1.276 ± 0.002
19.0	1.114 ± 0.000	323.67±0.01	19.50	1.263	1.261 ± 0.006	19.0	1.120 ± 0.000	323.65 ± 0.00	19.50	1.272	1.268 ± 0.006	1.264 ± 0.004
20.0	2.108 ± 0.000	318.96 ± 0.01	20,50	1.203	1.198±0.006	20.0	2.113±0.001	318.91 ± 0.01	20.50	1.201	1.204±0.006	1.201 ± 0.003
21.0	3.106±0.001	314.55 ± 0.02	21.50	1.194	1.200 ± 0.006	21.0	3.110±0.000	314.52 ± 0.01	21.50	1.200	1.206 ± 0.006	1.203 ± 0.003
23.0	5.110 ± 0.001	305.97 ± 0.01	22.50	1.207	1.206 ± 0.006	22.0	4.113 ± 0.001 5.112 ± 0.000	305.92 ± 0.01	22.50	1.213	1.212 ± 0.006	1.209 ± 0.003
23.0	2.228 ± 0.000	306.53+0.01				23.0	2.225 ± 0.001	306.56 ± 0.01				
24.0	3.234±0.000	302.35±0.00	23.50	1.201	1.204 ± 0.003	24.0	3.222+0.000	302.37±0.00	23.50	1.205	1.209±0.003	1.207 ± 0.003
25.0	4.232±0.000	298.31 ± 0.01	24.50	1.194	1.200 ± 0.003	25.0	4.221±0.000	298.30 ± 0.01	24,50	1.203	1.207±0.003	1.203±0.004
25.0	0.009 ± 0.001	299.02±0.01	25 50	1 001	1 010 1 0 005	25.0	0.100±0.001	299.05±0.01	05 50	1 000	1 200 1 0 005	1 000 1 0 000
26.0	1.008 ± 0.001	294.98±0.02	25.50	1,206	1,210±0.005	26.0	1.008±0.000	295.01 ±0.00	25.50	1.202	1.206 ± 0.005	1.208 ± 0.002
												Continuea) :-

Table 1.—Beckmann Readings, Mean Temperatures in °C., Flow Times and Calculated Values of (E/R) 1000 = $-T^2 (\Delta \ln \nu/\Delta T)/1000$ for n-Decane in Temperature Range of 9°C. to 90 °C., using $\Delta T = 1°C$.

(Table 1 Continued)

1 2 3	4	5	6	7	8	9	10	11	12	13	
27.0.2.014+0.000 291.00+0.0	26.50	1,212	1.216 ± 0.003	27.0	2 000-1-0.001	291 12 1 0 02	26.50	1.203	1.198 ± 0.005	1.204 ± 0.006	
27.0 2.014 ± 0.000 291.00 ± 0.0	27.50	1.200	1.207 ± 0.005	22.0	2.000 ± 0.001	291.12 ± 0.02	27.50	1.202	1.208 ± 0.005	1.208 ± 0.001	
$28.0 3.012 \pm 0.000 287.17 \pm 0.0$	28.50	1.192	1.197 ± 0.005	20.0	2.996±0.000	287.29±0.01	28.50	1.202	1.208 ± 0.005	1.203 ± 0.005	
$29.0 4.005 \pm 0.001 283.46 \pm 0.0$	29.50	1.217	1.212 ± 0.005	29.0	5.999±0.000	283.51±0.00	29.50	1.212	1.207 ± 0.005	1.209 ± 0.003	
$30.0 5.013 \pm 0.000 274.69 \pm 0.0$				30.0	5.002±0.000	279.76±0.01					
$30.0 0.092 \pm 0.001 1446.69 \pm 0.0$	30.50	1.212	1.200 ± 0.004	30.0	0.050 ± 0.001	1447.70±0.02	30.50	1.207	1.193 ± 0.004	1.196 ± 0.004	
$31.0 1.100 \pm 0.000 1427.03 \pm 0.0$	31.50	1.203	1.218 ± 0.004	31.0	1.047 ± 0.000	1428.94 ± 0.01	31.50	1.196	1.209 ± 0.004	1.213 ± 0.004	
$32.0 2.110 \pm 0.000 1409.08 \pm 0.0$	32.50	1.215	1.190 ± 0.004	32,0	2.043 ± 0.001	1410.77 ± 0.03	32.50	1.206	1.186 ± 0.004	1.188 ± 0.002	
$33.0 3.085 \pm 0.001 1391.33 \pm 0.0$	33.50	1.178	1.178 ± 0.004	33.0	3.052 ± 0.000	1392.52 ± 0.01	33.50	1.160	1.170 ± 0.004	1.174 ± 0.004	
$34.0 4.091 \pm 0.001 1373.90 \pm 0.0$	34.50	1,180	1.175 ± 0.004	34.00	4.051 ± 0.001	1375.41 ± 0.02	34.50	1.175	1.170 ± 0.004	1.172 ± 0.003	
$35.0 5.072 \pm 0.001 1357.20 \pm 0.0$	2			35.0	5.072 ± 0.001	1358.10 ± 0.02				Sec. Part	
$35.0 0.135 \pm 0.002 1356.95 \pm 0.0$	35.50	1,175	1.178 ± 0.005	35.0	0.069±0.001	1357.68 ± 0.02	35.50	1.169	1.172 ± 0.005	1.175 ± 0.003	
$36.0 1.125 \pm 0.000 1340.50 \pm 0.0$	36.50	1,177	1.174 ± 0.005	36.0	1.078 ± 0.002	1341.00 ± 0.03	36.50	1,178	1.175 ± 0.005	1.174 + 0.001	
$37.0 \ 2.101 \pm 0.001 \ 1324.51 \pm 0.001$	37.50	1,167	1.170 ± 0.005	37.0	2.078 ± 0.000	1324.62 ± 0.01	37.50	1.170	1.174 ± 0.005	1.172 ± 0.002	
$38.0 3.092 \pm 0.001 1308.73 \pm 0.0$	38.50	1 163	1.168 ± 0.005	38.0	3.082±0.001	1308.59 ± 0.02	38.50	1 170	1.175 ± 0.005	1.172 ± 0.003	
$39.0 4.089 \pm 0.000 1293.20 \pm 0.0$	39.50	1 172	1.167 ± 0.005	39.0	4.084 ± 0.000	1292.89±0.01	39.50	1 181	1 176±0.005	1.172 ± 0.005	
40.0 $5.072 \pm 0.001\ 1278.05 \pm 0.001$	2	1.1/2	1.10/_0.005	40.0	5.082±0.001	1278.17 ± 0.02	57.50	1.101	1.170_0.005	1.172_0.000	
40.0 0.083 ± 0.001 1282.17 ± 0.00	40 50	1 174	1 179 1 0 004	40.0	0.038 ± 0.001	1282.99±0.01	10 50	1 160	1 171 1 0 004	1 175 1 0 004	
41.0 1.093±0.000 1266.81±0.0	40,50	1.174	1.170 + 0.004	41.0	1.033 ± 0.000	1267.92 ± 0.01	40.50	1,100	1.171±0.004	1.175±0.004	
42.0 2.076 ± 0.001 1252.17 ± 0.001	41.50	1.1/1	1.170±0.004	42.0	2.041 ± 0.000	1252.81 ± 0.02	41.50	1.181	1.180±0.004	1.1/5±0.005	
43.0 3.065±0.001 1237.74±0.0	42.50	1.168	1.165 ± 0.004	43.0	3.044±0.002	1238.14 ± 0.03	42.50	1.170	1.173±0.004	1.169±0.004	
44.0 4.062±0.000 1223.43±0.0	43,50	1.170	1.177±0.004	44.0	4.043±0.000	1223.82 ± 0.01	43.50	1.168	1.172 ± 0.004	1.175±0.003	
45.0 5.042±0.001 1209.55±0.00	44.50	1.175	1.170 ± 0.004	45.0	5.044 ± 0.001	1209.51 ± 0.002	44.50	1.181	1.177 ± 0.004	1.173 ± 0.004	
45.0 -0.140±0.000 1207.70±0.0	0			45.0	-0.138 ± 0.001	1208.00±0.000					
46.0 0.883±0.001 1193.58±0.0	45.50	1.168	1.170 ± 0.004	46.0	0.851 ± 0.000	1194.30±0.01	45.50	1.171	1.173 ± 0.004	1.172 ± 0.001	
47.0 1.880±0.000 1179.96+0.0	46.50	1.176	1.178 ± 0.004	47.0	1.843+0.001	1180.86+0.03	46.50	1.165	1.167 ± 0.004	1.172 ± 0.005	
48.0 2.842+0.000 1167.31+0.0	47.50	1.159	1.155 ± 0.004	48.0	2,832+0,000	1167.94 ± 0.01	47.50	1.144	1.146 ± 0.004	1.151 ± 0.005	
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Table 1 (Continued)

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1	2	3	4	5	6	7	8	9	10	11	12	13
49.0	3 383-0 001	1154 63+0 02	48.50	1.140	1.148 ± 0.004	10.0	3 930 1 0 001	1155 14 1 0 02	48:50	1.14%	°1.157±0.004	1.152 ± 0.005
50.0	4.816 ± 0.000	1134.03 ± 0.02 $1142 \pm 17 \pm 0.01$	49.50 y	1.152	1.147 ± 0.004	49.0 50.0	3.830 ± 0.001	1153.14 ± 0.02 1143.57 ± 0.01	49.50	1.156	1.151 ± 0.004	1.149±0.002
50.0	0 160+0 000	$1141 \pm 82 \pm 0.02$				50.0	4.020±0.001	1141 12 0 02	10. 0th	1.92		
50.0	1 125 1 0 001	1141 ± 0.02	50.50	1.158	1.158 ± 0.004	50.0	0.142±0.001	1141.13±0.02	50.50	1.149	1.151 ± 0.004	1.155 ± 0.004
52.0	2 102 + 0 000	1129.09±0.02	51.50	1.157	1.154 ± 0.004	51.0	1.124±0.000	1128.91±0.01	51.50	1.152	1.151 ± 0.004	1.153 ± 0.002
52.0	2.103±0.000	1117.63 ± 0.01	52.50	1.145	1.148 ± 0.004	52.0	2.105 ± 0.001	1117.28 ± 0.02	52,50	1.152	1.155 ± 0.004	1.152 ± 0.003
53.0	3.064±0.001	1106.13 ± 0.02	53.50	1.149	1.155 ± 0.004	53.0	3.096 ± 0.000	1105.34 ± 0.01	53.50	14.45	1.150 ± 0.004	1.153±0.003
54.0	4.062 ± 0.000	1094.26 ± 0.02	54.50	1.159	1.152 ± 0.004	54.0	4.073±0.001	1093.81 ± 0.02	54.50	1.155	1.153 ± 0.004	1.152 ± 0.001
55.0	5.030 ± 0.000	1082.88 ± 0.01				55.0	5.030 ± 0.000	1080.59 ± 0.01				
55.0	-0.160 ± 0.000	1083.86 ± 0.01	55.50	1.157	1.156 ± 0.005	55.0	-0.140 ± 0.001	1083.39 ± 0.02	55.50	1,145	1.144 ± 0.005	1.150±0.006
56.0	0.842 ± 0.002	1072.30 ± 0.02	56.50	1.153	1.156+0.005	56.0	0.841 ± 0.000	1072.18 ± 0.02	56.50	1.144	1.150 ± 0.005	1.153 ± 0.003
57.0	1.822 ± 0.000	1061.77 ± 0.01	57.00	1,146	1.149+0.005	57.0	1.794 ± 0.001	1061.48 ± 0.03	57.50	1.156	1.158 ± 0.005	1.154+0.005
58.0	2.818 ± 0.001	1050.74 ± 0.00	58,50	1,123	1.130+0.005	58.0	2.762 ± 0.001	1050.63 ± 0.02	58.50	1.115	1.122 ± 0.005	1.126-1-0.004
59.0	3.759 ± 0.000	1040.69±0.01	59.50	1 105	1 100+0 005	59.0	3.750±0.000	1040.16 ± 0.00	59.50	1 109	1 105+0 005	1.103+0.002
60.50	0 5.247±0.001	1025.38 ± 0.02		1.105	1.100±0.003	60.50	5.247 ± 0.001	1024.80±0.02		1.107	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	N 7 37701
60.00	0.106 ± 0.001	1029.44 ± 0.02	60 50	1 107	1 110 1 0 004	60.0	0.112 ± 0.001	1029.18±0.01	60.50	1 103	1 104+0 004	1 107-10.003
61.0	1.099 ± 0.000	1019.32 ± 0.01	61 50	1.107	1.10-0.004	61.0	1.080 ± 0.000	1019.45 ± 0.01	61 50	1,103	1.009 1.0.004	1.107 ± 0.003
62.0	2.093 ± 0.002	1009.33 ± 0.02	62 50	1.108	1.105±0.004	62.0	2.079 ± 0.001	1009.47±0.02	61.50	1.102	1.007 + 0.004	1.102±0.003
63.0	3.095 ± 0.000	1000.50 ± 0.01	62.50	1.097	1.100±0.004	63.0	3.087 ± 0.001	1000.73 ± 0.02	62.50	1.094	1.097±0.004	1.090±0.002
64.0	4.088 ± 0.001	990.97±0.02	63.50	1.100	1.105 ± 0.004	64.0	4.077±0.000	991.21±0.00	63.50	1.095	1.100±0.004	1.105±0.003
65.0	5.063 ± 0.000	981.65±0.01	64.50	1,105	1.100 ± 0.004	65.0	5.062 ± 0.001	981.72±0.02	64.50	1.113	1.108 ± 0.004	1.104 ± 0.004
65.0	-0.008 ± 0.001	981.96±0.02	1.11			65.0	0.000 ± 0.002	981.97±0.03				
65.0	1.000 ± 0.000	972.69±0.01	65.50	1.098	1.100 ± 0.006	66.0	0.999±0.000	973.03±0.01	65.50	1.103	1.105 ± 0.006	1.102 ± 0.003
67.0	1.966 ± 0.001	963.77±0.02	66.50	1.100	1.101 ± 0.006	67.0	1.990 ± 0.001	963.90 ± 0.02	66.50	1.107	1.110 ± 0.006	1.105 ± 0.005
68.0	2.949 ± 0.001	954.98+0.02	67.50	1.096	1.101 ± 0.006	68.0	2.972 ± 0.001	955.17+0.02	67.50	1.086	1.091 ± 0.006	1.096 ± 0.005
	Angla		68,50	1.100	1.100±0.006				68.50	1.104	1.107±0.006	1.104 ± 0.004
											· · · · · · ·	Continued) .

(Continued) :-

(Table 1 Continued)

1	2	3	4	5	6	7	8	9	10	11	12	13
69.	$0 3.942 \pm 0.000$	946.05±0.02	60 50	1 100	1 105 0 006	69.0	3.950 ± 0.002	946.30±0.03	60 50	1 104	1 100 1 0 000	1 102 1 0 002
70.	0 4.917 \pm 0.002	937.39 ± 0.03	69.50	1.109	1.105±0.006	70.0	4.952 ± 0.000	937.44±0.01	09.50	1,104	1.100±0.006	1.102 ± 0.003
70.	0.103 ± 0.001	927.85 ± 0.02	70.50	1 100	1 102 0 006	70.0	0.113 ± 0.002	937.66±0.02	70 50	1 089	1 091 1 0 006	1 007 1 0 000
71.	$0 1.076 \pm 0.000$	929.39 ± 0.01	70.50	1.100	1.102 ± 0.006	71.0	1.099±0.000	929.18±0.01	70.50	1 111	1.1091±0.006	1.106 + 0.002
72.	$0 2.059 \pm 0.002$	920.92±0.03	72.50	1.003	1.097 ± 0.005	72.0	2.092 ± 0.001	920.61±0.02	72.50	1.008	1.00 ± 0.000	1.100 ± 0.003
73.	$0 3.034 \pm 0.000$	$912.73 {\pm} 0.01$	72.50	1.053	1.097 ± 0.005	73.0	3.088±0.000	912.20±0.01	72.50	1.050	1.092 ± 0.006	1.095 ± 0.003
74.	$0 4.037 \pm 0.001$	904.76 ± 0.02	73,50	1.055	1.035 ± 0.000	74.0	4.061±0.000	$904.41 {\pm} 0.01$	74.50	1.059	1.004 ± 0.006	1.059 ± 0.003
75.	05.029 ± 0.002	897.10±0.02	74.50	1.031	1.040±0.000	75.0	5.0.3±0.002	896.65±0.03	74.50	1.058	1.035±0.000	1.050±0.003
75.	0.008 ± 0.001	897.10 ± 0.02	75 50	1 027	1 032 1 0 007	75.0	$0.006 {\pm} 0.001$	897.05±0.02	75 50	1 032	1 037 + 0 007	1 035 1 0 002
76.	$0 1.086 \pm 0.000$	889.72 ± 0.01	76.50	1.027	1.049 ± 0.007	76.0	0.979 ± 0.002	889.67±0.04	76.50	1.052	1.057 ± 0.007	1.053 ± 0.002
77.	$0 2.049 \pm 0.001$	882.37±0.02	77.50	1 049	1.049 ± 0.007	77.0	1.941 ± 0.001	882.32 ± 0.02	77.50	1.057	1.053 ± 0.007	1.052 ± 0.003
78.	$0 3.050 \pm 0.000$	874.87 ± 0.01	78.50	1.073	1.033 ± 0.007	78.0	2.940 ± 0.001	874.78±0.01	78.50	1.078	1.083+0.007	1.037 ± 0.004
79.	$0 4.005 \pm 0.001$	867.65±0.02	79.50	1 108	1.073 ± 0.007	79.0	3.940±0.000	867.18 ± 0.01	70.50	1,103	1.003 ± 0.007 1.098 ± 0.007	1.000 ± 0.003
80.	$0 5.004 \pm 0.002$	859.94±0.03	77.30	1,100	1.105_0.007	.80.0	4.905 ± 0.001	859.77±0.03	19.00	11100	1.000_0.000	1.101_0.005
80.	0.116 ± 0.001	860.21±0.02	80.50	1 085	1 088+0 007	80.0	$0.110 {\pm} 0.001$	860.17±0.01	80.50	1.093	1.096 ± 0.007	1 092+0 004
81.	$0 1.110 \pm 0.001$	852.83 ± 0.01	81.50	1.080	1.000 ± 0.007	81.0	1.005 ± 0.002	852.74±0.02	81.50	1.085	1.082 ± 0.007	1.092 ± 0.004
82.	$0 2.078 \pm 0.001$	845.73±0.01	82 50	1.042	1.045 ± 0.007	82.0	$1.978 {\pm} 0.001$	845.61±0.01	82.50	1.054	1.058 ± 0.007	1.051 ± 0.007
83.	$0 3.055 \pm 0.001$	838.95 ± 0.02	83.00	1.026	1.031 ± 0.007	83.0	$2.953 {\pm} 0.001$	838.77±0.02	83.50	1.028	1.043 ± 0.007	1.037 ± 0.006
84.	$0 4.010 \pm 0.000$	832.51 ± 0.01	84.50	1.057	1.051 ± 0.007	84.0	3.919±0.000	832.25±0.01	84.50	1.051	1.047+0.007	1.057 ± 0.005
85.	$0 4.998 \pm 0.001$	825.74 ± 0.02	01.50	1.007	1.000_0.007	85,0	4.994±0.002	825.61±0.02	01100		TION TOTON	1.002_0.000
85.	0.008 ± 0.001	826.17 ± 0.01	85.50	1.054	1 050+0 006	85.0	0.103 ± 0.001	826.23±0.01	85.50	1.069	1.055 ± 0.006	1.052 ± 0.003
86.	0.996 ± 0.002	$819.51 {\pm} 0.02$	86.50	1 072	1.069 ± 0.006	86.0	1.076 ± 0.000	819.64±0.00	86.50	1.072	1.068+0.006	1.069 ± 0.001
87.	$0 1.962 \pm 0.001$	$812.98 {\pm} 0.02$	87.50	1.087	1.092 ± 0.000	87.0	2.064±0.002	812.96±0.02	87.50	1.096	1.110+0.006	1.096 ± 0.005
88.	$0 2.967 \pm 0.000$	806.16 ± 0.00	88.50	1.097	1.099 ± 0.006	88.0	3.019±0.000	806.44±0.01	88.50	1.084	1.087 ± 0.006	1.092 ± 0.005
89.	3.966 ± 0.002	799.43 ± 0.02	89.50	1.085	1.080 ± 0.006	89.0	4.009±0.001	799.85±0.01	89.50	1.096	1.091+0.006	1.086+0.005
90.	4.932 ± 0.001	793.12 ± 0.01	07.00	1.005	1.000_0.000	90.0	4.987 ± 0.002	793.34 ± 0.02				11.300.L 01.000

TAYEB M. QURESHI, S.A. BARI AND M.M. QURASHI



Fig. 1.—Graphs showing the variation of the activation energy of viscous flow E/R with temperature for n-decane; the upper graph (solid circles and crosses) is the previously reported data using the measuring interval of 2°C. The lower graph (hollow circles) is the data obtained by using viscometer No. '0' and a measuring thermal interval of 1°C. This graph provides more details, and shows a regular series of steps, followed by cyclic variation above $73\pm2^{\circ}C$.

These results on n-octane are somewhat out of the run, so it was considered desirable to study one of its isomeric forms to determine whether this feature is characteristic of the eight aliphatic carbon atoms only, or also depends upon factors such Iso-octane (2:2:4 trimethyl as configuration. pentane, $(CH_3)C-CH_2-CH(CH_3)_2$ of special spectroscopic grade (BDH) was considered for this purpose; it has lower freezing point (-107.3°C.) and boiling point (99.2°C.) as compared to noctane. The viscosity measurements were carried out with viscometer No 'O', exactly as for n-decane and n-octane, the time of flow ranging from 1100 seconds at lower temperatures to 600 seconds at higher temperatures. The measurements were carried out in the range of 5° to 73°C. at the interval of 1° C., and the values of (E/R)/1000 against temperature in °C. obtained during heating and cooling sequences are collected in Table 2(b), together with overall means and r.m.s. deviations (for the groups of measurements of 5) which comes out to be of the order of \pm 0.004 units. The solid circles in Fig. 2(bottom) show these values plotted against temperature in °C., and a smooth curve is drawn through all these

points. This curve is different from all the previous work so far reported, in so far as at lower temperatures it assumes a cyclic form, with peak-to-peak amplitude of the order of 0.04 units of $E/R \div$ 1000 and period 6°C., while above 53°C., it undergoes a sudden change and jumps upwards to a horizontal straight line going upto the last experimental point at 73°C., which is very near to its boiling point (99.2°C.). Secondly the E/R values are somewhat higher than n-octane by 0.05 units, and the mean values of E appears to go through an absolute minima in the neighbourhood of 30°C. It is also notable that the transition from sinusoidal variation to the horizontal straight line occurs at the same temperature of 54°C., where the transition in n-octane took place in reversed order.

Experiment with n-Hexane (C_6H_{14})

To study further these interesting phenomena in the activation energy E in the lighter hydrocarbons, experiments were carried out on nhexane C_6H_{14} , (special for spectroscopy BDH) having freezing point-95°C. and boiling point 68.7°C. This is highly volatile and therefore

eating quence Cooling sequence 2 ± 0.004 0.971 ± 0.00 8 ± 0.004 0.963 ± 0.00 4 ± 0.004 0.970 ± 0.00 8 ± 0.003 0.972 ± 0.00 3 ± 0.003 0.972 ± 0.00 3 ± 0.003 0.968 ± 0.003 3 ± 0.003 0.968 ± 0.003 3 ± 0.003 0.968 ± 0.003 6 ± 0.003 0.968 ± 0.000 6 ± 0.004 0.968 ± 0.000 8 ± 0.004 0.970 ± 0.002 2 ± 0.004 0.967 ± 0.002 0 ± 0.004 0.967 ± 0.002 0 ± 0.004 0.967 ± 0.002 0 ± 0.004 0.967 ± 0.002 0 ± 0.003 0.962 ± 0.002 0 ± 0.003 0.966 ± 0.002	$\begin{array}{c} \mbox{Mean}\\ & & 0.966 \pm 0.005\\ 4 & 0.965 \pm 0.002\\ 4 & 0.967 \pm 0.003\\ 3 & 0.970 \pm 0.002\\ 3 & 0.966 \pm 0.002\\ 4 & 0.972 \pm 0.004\\ 4 & 0.964 \pm 0.006\\ 4 & 0.964 \pm 0.006\\ 4 & 0.963 \pm 0.001\\ 4 & 0.963 \pm 0.003\\ 4 & 0.955 \pm 0.005\\ 4 & 0.965 \pm 0.003\\ 3 & 0.966 \pm 0.003\\ 3 & 0.965 \pm 0.003\\ 3 & 0.961 \pm 0.003\\ 3 & 0.961 \pm 0.003\\ \end{array}$	41.5 42.5 43.5 44.5 45.5 44.5 45.5 46.5 47.5 48.5 50.0 51.5 52.5 53.5 54.5 55.5 56.5 57.5 58.5 59.5 60.5 60.5 61.5	$\begin{array}{c} \begin{array}{c} \mbox{Heating sequence} \\ \mbox{sequence} \\ \hline \mbox{0.980} \pm 0.005 \\ \mbox{0.968} \pm 0.005 \\ \mbox{0.968} \pm 0.005 \\ \mbox{0.968} \pm 0.005 \\ \mbox{0.968} \pm 0.004 \\ \mbox{0.962} \pm 0.004 \\ \mbox{0.966} \pm 0.004 \\ \mbox{0.966} \pm 0.005 \\ \mbox{0.966} \pm 0.005 \\ \mbox{0.963} \pm 0.005 \\ \mbox{0.955} \pm 0.005 \\ \mbox{0.955} \pm 0.005 \\ \mbox{0.952} \pm 0.005 \\ \mbox{0.952} \pm 0.005 \\ \mbox{0.969} \pm 0.005 \\ \mbox{0.969} \pm 0.005 \\ \mbox{0.966} \pm 0.005 \\ \mbox{0.962} \pm 0.006 \\ \mbox{0.928} \pm 0.006 \\ 0.92$	$\begin{array}{c} \text{Cooling} \\ \text{sequence} \\ \hline \\ 0.972 \pm 0.005 \\ 0.964 \pm 0.005 \\ 0.965 \pm 0.005 \\ 0.963 \pm 0.005 \\ 0.962 \pm 0.004 \\ 0.964 \pm 0.004 \\ 0.974 \pm 0.004 \\ 0.974 \pm 0.004 \\ 0.970 \pm 0.004 \\ 0.964 \pm 0.005 \\ 0.966 \pm 0.005 \\ 0.966 \pm 0.005 \\ 0.969 \pm 0.005 \\ 0.948 \pm 0.005 \\ 0.948 \pm 0.005 \\ 0.958 \pm 0.005 \\ 0.962 \pm 0.005 \\ 0.928 \pm 0.006 \\ 0.922 \pm 0.006 \\ \end{array}$	Mean 0.976 \pm 0.004 0.966 \pm 0.002 0.963 \pm 0.002 0.964 \pm 0.001 0.965 \pm 0.002 0.970 \pm 0.000 0.968 \pm 0.000 0.965 \pm 0.000 0.965 \pm 0.001 0.965 \pm 0.001 0.965 \pm 0.003 0.945 \pm 0.003 0.945 \pm 0.003 0.945 \pm 0.003 0.945 \pm 0.003 0.955 \pm 0.003 0.965 \pm 0.004 0.965 \pm 0.004 0.965\pm0.004 0.965 \pm 0.004 0.965\pm0.004 0.965 \pm 0.004 0.965\pm0.004 0.965\pm0.004 0.965\pm0.004 0.965\pm0.004 0.965\pm0.004 0.965\pm0.004 0.965\pm0.004 0.965\pm0.004 0.965\pm0.005 0.965\pm0.00
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 41.5\\ 42.5\\ 43.5\\ 44.5\\ 45.5\\ 46.5\\ 47.5\\ 48.5\\ 49.5\\ 50.0\\ 51.5\\ 52.5\\ 53.5\\ 54.5\\ 55.5\\ 54.5\\ 55.5\\ 56.5\\ 57.5\\ 58.5\\ 59.5\\ 60.5\\ 61.5\\ \end{array}$	$\begin{array}{c} 0.980 \pm 0.005\\ 0.968 \pm 0.005\\ 0.968 \pm 0.005\\ 0.960 \pm 0.005\\ 0.964 \pm 0.005\\ 0.968 \pm 0.004\\ 0.975 \pm 0.004\\ 0.968 \pm 0.004\\ 0.966 \pm 0.005\\ 0.966 \pm 0.005\\ 0.963 \pm 0.005\\ 0.963 \pm 0.005\\ 0.955 \pm 0.005\\ 0.937 \pm 0.005\\ 0.937 \pm 0.005\\ 0.952 \pm 0.005\\ 0.969 \pm 0.005\\ 0.969 \pm 0.005\\ 0.966 \pm 0.005\\ 0.968 \pm 0.006\\ 0.928 \pm 0.006\\$	$\begin{array}{c} 0.972 \pm 0.005\\ 0.964 \pm 0.005\\ 0.965 \pm 0.005\\ 0.963 \pm 0.005\\ 0.962 \pm 0.004\\ 0.964 \pm 0.004\\ 0.974 \pm 0.004\\ 0.974 \pm 0.004\\ 0.970 \pm 0.004\\ 0.966 \pm 0.005\\ 0.966 \pm 0.005\\ 0.966 \pm 0.005\\ 0.948 \pm 0.005\\ 0.948 \pm 0.005\\ 0.958 \pm 0.005\\ 0.962 \pm 0.005\\ 0.928 \pm 0.006\\ 0.922 \pm 0.006\\ 0.922 \pm 0.006\\ \end{array}$	$\begin{array}{c} 0.976 \pm 0.004 \\ 0.966 \pm 0.007 \\ 0.963 \pm 0.007 \\ 0.963 \pm 0.007 \\ 0.965 \pm 0.001 \\ 0.965 \pm 0.002 \\ 0.941 \pm 0.003 \\ 0.955 \pm 0.003 \\ 0.965 \pm 0.004 \\ 0.964 \pm 0.003 \\ 0.922 \pm 0.006 \\ 0.925 \pm 0.004 \\ 0.925 \pm 0.003 \\ 0.925 \pm 0.004 \\ 0.925 \pm$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 41.3\\ 42.5\\ 43.5\\ 44.5\\ 44.5\\ 45.5\\ 46.5\\ 47.5\\ 48.5\\ 50.0\\ 51.5\\ 52.5\\ 53.5\\ 55.5\\ 55.5\\ 55.5\\ 56.5\\ 57.5\\ 58.5\\ 59.5\\ 59.5\\ 60.5\\ 61.5\\ \end{array}$	$\begin{array}{c} 0.968 \pm 0.005\\ 0.968 \pm 0.005\\ 0.968 \pm 0.005\\ 0.966 \pm 0.005\\ 0.968 \pm 0.004\\ 0.975 \pm 0.004\\ 0.975 \pm 0.004\\ 0.962 \pm 0.004\\ 0.966 \pm 0.004\\ 0.966 \pm 0.005\\ 0.963 \pm 0.005\\ 0.963 \pm 0.005\\ 0.955 \pm 0.005\\ 0.937 \pm 0.005\\ 0.937 \pm 0.005\\ 0.952 \pm 0.005\\ 0.969 \pm 0.005\\ 0.969 \pm 0.005\\ 0.960 \pm 0.005\\ 0.966 \pm 0.005\\ 0.966 \pm 0.005\\ 0.966 \pm 0.005\\ 0.966 \pm 0.005\\ 0.916 \pm 0.006\\ 0.928 \pm 0.006\\$	$\begin{array}{c} 0.972\pm0.005\\ 0.964\pm0.005\\ 0.965\pm0.005\\ 0.965\pm0.005\\ 0.962\pm0.004\\ 0.962\pm0.004\\ 0.974\pm0.004\\ 0.974\pm0.004\\ 0.970\pm0.004\\ 0.964\pm0.005\\ 0.966\pm0.005\\ 0.966\pm0.005\\ 0.969\pm0.005\\ 0.948\pm0.005\\ 0.948\pm0.005\\ 0.958\pm0.005\\ 0.962\pm0.005\\ 0.962\pm0.005\\ 0.962\pm0.005\\ 0.928\pm0.006\\ 0.922\pm0.006\\ 0.922\pm0.006\\ \end{array}$	$\begin{array}{c} 0.966\pm 0.00;\\ 0.966\pm 0.00;\\ 0.963\pm 0.00;\\ 0.965\pm 0.00;\\ 0.965\pm 0.00;\\ 0.970\pm 0.00;\\ 0.966\pm 0.00;\\ 0.966\pm 0.00;\\ 0.965\pm 0.00;\\ 0.965\pm 0.00;\\ 0.965\pm 0.00;\\ 0.965\pm 0.00;\\ 0.945\pm 0.00;\\ 0.955\pm 0.00;\\ 0.955\pm 0.00;\\ 0.955\pm 0.00;\\ 0.965\pm 0.00;\\ 0.925\pm 0.$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 42.3\\ 43.5\\ 44.5\\ 44.5\\ 45.5\\ 46.5\\ 47.5\\ 48.5\\ 49.5\\ 50.0\\ 51.5\\ 52.5\\ 53.5\\ 52.5\\ 53.5\\ 55.5\\ 55.5\\ 56.5\\ 57.5\\ 58.5\\ 59.5\\ 59.5\\ 60.5\\ 61.5\\ \end{array}$	$\begin{array}{c} 0.968 \pm 0.005\\ 0.960 \pm 0.005\\ 0.964 \pm 0.005\\ 0.968 \pm 0.004\\ 0.975 \pm 0.004\\ 0.962 \pm 0.004\\ 0.968 \pm 0.004\\ 0.968 \pm 0.004\\ 0.966 \pm 0.005\\ 0.966 \pm 0.005\\ 0.963 \pm 0.005\\ 0.963 \pm 0.005\\ 0.955 \pm 0.005\\ 0.942 \pm 0.005\\ 0.952 \pm 0.005\\ 0.952 \pm 0.005\\ 0.969 \pm 0.005\\ 0.969 \pm 0.005\\ 0.966 \pm 0.005\\ 0.966 \pm 0.005\\ 0.966 \pm 0.005\\ 0.916 \pm 0.006\\ 0.928 \pm 0.006\\$	$\begin{array}{c} 0.964 \pm 0.005 \\ 0.965 \pm 0.005 \\ 0.963 \pm 0.005 \\ 0.962 \pm 0.004 \\ 0.964 \pm 0.004 \\ 0.974 \pm 0.004 \\ 0.970 \pm 0.004 \\ 0.970 \pm 0.005 \\ 0.966 \pm 0.005 \\ 0.969 \pm 0.005 \\ 0.969 \pm 0.005 \\ 0.948 \pm 0.005 \\ 0.948 \pm 0.005 \\ 0.960 \pm 0.005 \\ 0.967 \pm 0.005 \\ 0.967 \pm 0.005 \\ 0.962 \pm 0.005 \\ 0.928 \pm 0.006 \\ 0.922 \pm 0.006 \\ 0.922 \pm 0.006 \\ \end{array}$	$\begin{array}{c} 0.963 \pm 0.00;\\ 0.963 \pm 0.00;\\ 0.964 \pm 0.00;\\ 0.965 \pm 0.00;\\ 0.966 \pm 0.00;\\ 0.966 \pm 0.00;\\ 0.965 \pm 0.00;\\ 0.941 \pm 0.00;\\ 0.955 \pm 0.00;\\ 0.955 \pm 0.00;\\ 0.965 \pm 0.00;\\ 0.925 \pm 0.00;\\ 0.922 \pm 0.00;\\ 0.925 \pm 0.00;\\$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	43.3 44.5 45.5 46.5 47.5 48.5 49.5 50.0 51.5 52.5 53.5 54.5 55.5 56.5 57.5 58.5 59.5 60.5 60.5 61.5	$\begin{array}{c} 0.960 \pm 0.005\\ 0.964 \pm 0.005\\ 0.968 \pm 0.004\\ 0.975 \pm 0.004\\ 0.962 \pm 0.004\\ 0.968 \pm 0.004\\ 0.966 \pm 0.005\\ 0.963 \pm 0.005\\ 0.963 \pm 0.005\\ 0.963 \pm 0.005\\ 0.955 \pm 0.005\\ 0.937 \pm 0.005\\ 0.952 \pm 0.005\\ 0.969 \pm 0.005\\ 0.969 \pm 0.005\\ 0.966 \pm 0.005\\ 0.966 \pm 0.005\\ 0.966 \pm 0.005\\ 0.966 \pm 0.005\\ 0.962 \pm 0.006\\ 0.928 \pm 0.006\\$	$\begin{array}{c} 0.963 \pm 0.005\\ 0.963 \pm 0.005\\ 0.962 \pm 0.004\\ 0.974 \pm 0.004\\ 0.974 \pm 0.004\\ 0.970 \pm 0.004\\ 0.964 \pm 0.005\\ 0.966 \pm 0.005\\ 0.966 \pm 0.005\\ 0.969 \pm 0.005\\ 0.948 \pm 0.005\\ 0.958 \pm 0.005\\ 0.960 \pm 0.005\\ 0.967 \pm 0.005\\ 0.962 \pm 0.005\\ 0.928 \pm 0.006\\ 0.922 \pm 0.006\\ 0.922 \pm 0.006\\ \end{array}$	$\begin{array}{c} 0.963 \pm 0.00, \\ 0.964 \pm 0.00, \\ 0.965 \pm 0.00, \\ 0.966 \pm 0.00, \\ 0.966 \pm 0.00, \\ 0.965 \pm 0.00, \\ 0.945 \pm 0.00, \\ 0.941 \pm 0.00, \\ 0.955 \pm 0.00, \\ 0.965 \pm 0.00, \\ 0.965 \pm 0.00, \\ 0.964 \pm 0.00, \\ 0.922 \pm 0.00, \\ 0.925 \pm$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	44.3 45.5 46.5 47.5 48.5 50.0 51.5 52.5 53.5 54.5 55.5 56.5 57.5 58.5 59.5 60.5 60.5 61.5	$\begin{array}{c} 0.968\pm 0.004\\ 0.968\pm 0.004\\ 0.975\pm 0.004\\ 0.962\pm 0.004\\ 0.962\pm 0.004\\ 0.960\pm 0.004\\ 0.966\pm 0.005\\ 0.966\pm 0.005\\ 0.963\pm 0.005\\ 0.955\pm 0.005\\ 0.942\pm 0.005\\ 0.937\pm 0.005\\ 0.952\pm 0.005\\ 0.969\pm 0.005\\ 0.969\pm 0.005\\ 0.966\pm 0.005\\ 0.966\pm 0.005\\ 0.916\pm 0.006\\ 0.928\pm 0.$	$\begin{array}{c} 0.963 \pm 0.005\\ 0.962 \pm 0.004\\ 0.964 \pm 0.004\\ 0.974 \pm 0.004\\ 0.970 \pm 0.004\\ 0.970 \pm 0.005\\ 0.966 \pm 0.005\\ 0.966 \pm 0.005\\ 0.948 \pm 0.005\\ 0.948 \pm 0.005\\ 0.958 \pm 0.005\\ 0.962 \pm 0.005\\ 0.962 \pm 0.005\\ 0.962 \pm 0.005\\ 0.962 \pm 0.005\\ 0.928 \pm 0.006\\ 0.922 \pm 0.006\\ 0.922 \pm 0.006\\ \end{array}$	$\begin{array}{c} 0.96\pm 0.00\\ 0.96\pm 0.00\\ 0.965\pm 0.00\\ 0.968\pm 0.00\\ 0.966\pm 0.00\\ 0.965\pm 0.00\\ 0.965\pm 0.00\\ 0.965\pm 0.00\\ 0.965\pm 0.00\\ 0.965\pm 0.00\\ 0.945\pm 0.00\\ 0.945\pm 0.00\\ 0.945\pm 0.00\\ 0.955\pm 0.00\\ 0.965\pm 0.00\\ 0.964\pm 0.00\\ 0.964\pm 0.00\\ 0.922\pm 0.00\\ 0.925\pm 0.00\\ $
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	43.3 46.5 47.5 48.5 50.0 51.5 52.5 53.5 54.5 55.5 56.5 57.5 58.5 59.5 60.5 60.5 61.5	$\begin{array}{c} 0.968 \pm 0.004\\ 0.975 \pm 0.004\\ 0.962 \pm 0.004\\ 0.966 \pm 0.004\\ 0.966 \pm 0.005\\ 0.963 \pm 0.005\\ 0.963 \pm 0.005\\ 0.955 \pm 0.005\\ 0.952 \pm 0.005\\ 0.952 \pm 0.005\\ 0.952 \pm 0.005\\ 0.969 \pm 0.005\\ 0.960 \pm 0.005\\ 0.966 \pm 0.005\\ 0.916 \pm 0.006\\ 0.928 \pm 0.006\\$	$\begin{array}{c} 0.962\pm 0.004\\ 0.964\pm 0.004\\ 0.974\pm 0.004\\ 0.974\pm 0.004\\ 0.970\pm 0.004\\ 0.964\pm 0.005\\ 0.966\pm 0.005\\ 0.969\pm 0.005\\ 0.948\pm 0.005\\ 0.948\pm 0.005\\ 0.958\pm 0.005\\ 0.960\pm 0.005\\ 0.962\pm 0.005\\ 0.962\pm 0.005\\ 0.962\pm 0.005\\ 0.928\pm 0.006\\ 0.922\pm 0.006\\ \end{array}$	$\begin{array}{c} 0.963 \pm 0.00,\\ 0.970 \pm 0.00,\\ 0.968 \pm 0.00,\\ 0.965 \pm 0.00,\\ 0.945 \pm 0.00,\\ 0.945 \pm 0.00,\\ 0.955 \pm 0.00,\\ 0.965 \pm 0.00,\\ 0.965 \pm 0.00,\\ 0.964 \pm 0.00,\\ 0.925 \pm 0.00,\\$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	40.5 47.5 48.5 49.5 50.0 51.5 52.5 53.5 54.5 55.5 56.5 57.5 58.5 59.5 60.5 60.5 61.5	$\begin{array}{c} 0.975\pm 0.004\\ 0.962\pm 0.004\\ 0.968\pm 0.004\\ 0.966\pm 0.005\\ 0.963\pm 0.005\\ 0.963\pm 0.005\\ 0.955\pm 0.005\\ 0.942\pm 0.005\\ 0.937\pm 0.005\\ 0.952\pm 0.005\\ 0.969\pm 0.005\\ 0.960\pm 0.005\\ 0.966\pm 0.005\\ 0.916\pm 0.006\\ 0.928\pm 0.$	$\begin{array}{c} 0.964 \pm 0.004 \\ 0.974 \pm 0.004 \\ 0.964 \pm 0.004 \\ 0.960 \pm 0.005 \\ 0.969 \pm 0.005 \\ 0.969 \pm 0.005 \\ 0.948 \pm 0.005 \\ 0.948 \pm 0.005 \\ 0.948 \pm 0.005 \\ 0.967 \pm 0.005 \\ 0.967 \pm 0.005 \\ 0.962 \pm 0.005 \\ 0.928 \pm 0.006 \\ 0.922 \pm 0.006 \\ 0.922 \pm 0.006 \end{array}$	$\begin{array}{c} 0.976\pm0.004\\ 0.968\pm0.000\\ 0.965\pm0.005\\ 0.965\pm0.005\\ 0.965\pm0.001\\ 0.965\pm0.007\\ 0.945\pm0.007\\ 0.945\pm0.007\\ 0.945\pm0.003\\ 0.955\pm0.003\\ 0.955\pm0.003\\ 0.965\pm0.004\\ 0.964\pm0.003\\ 0.964\pm0.004\\ 0.922\pm0.006\\ 0.925\pm0.003\\ 0.925\pm0.003$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	47.5 48.5 49.5 50.0 51.5 52.5 53.5 54.5 55.5 56.5 58.5 59.5 60.5 60.5 61.5	$\begin{array}{c} 0.962\pm 0.004\\ 0.968\pm 0.004\\ 0.966\pm 0.004\\ 0.966\pm 0.005\\ 0.963\pm 0.005\\ 0.955\pm 0.005\\ 0.955\pm 0.005\\ 0.937\pm 0.005\\ 0.937\pm 0.005\\ 0.952\pm 0.005\\ 0.969\pm 0.005\\ 0.960\pm 0.005\\ 0.966\pm 0.005\\ 0.916\pm 0.006\\ 0.928\pm 0.006\\ 0.928\pm 0.006\end{array}$	$\begin{array}{c} 0.974 \pm 0.004 \\ 0.964 \pm 0.004 \\ 0.970 \pm 0.004 \\ 0.964 \pm 0.005 \\ 0.966 \pm 0.005 \\ 0.969 \pm 0.005 \\ 0.948 \pm 0.005 \\ 0.948 \pm 0.005 \\ 0.958 \pm 0.005 \\ 0.960 \pm 0.005 \\ 0.967 \pm 0.005 \\ 0.962 \pm 0.005 \\ 0.928 \pm 0.006 \\ 0.922 \pm 0.006 \\ 0.922 \pm 0.006 \end{array}$	$\begin{array}{c} 0.968 \pm 0.001\\ 0.966 \pm 0.002\\ 0.965 \pm 0.002\\ 0.965 \pm 0.002\\ 0.965 \pm 0.002\\ 0.965 \pm 0.002\\ 0.945 \pm 0.002\\ 0.941 \pm 0.002\\ 0.955 \pm 0.002\\ 0.965 \pm 0.002\\ 0.964 \pm 0.002\\ 0.964 \pm 0.002\\ 0.922 \pm 0.006\\ 0.925 \pm 0.002\\ 0.925 \pm 0.002\\$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	48.5 49.5 50.0 51.5 52.5 53.5 54.5 55.5 56.5 57.5 58.5 59.5 60.5 60.5 61.5	$\begin{array}{c} 0.968 \pm 0.004\\ 0.960 \pm 0.004\\ 0.966 \pm 0.005\\ 0.963 \pm 0.005\\ 0.955 \pm 0.005\\ 0.955 \pm 0.005\\ 0.942 \pm 0.005\\ 0.937 \pm 0.005\\ 0.952 \pm 0.005\\ 0.969 \pm 0.005\\ 0.966 \pm 0.005\\ 0.966 \pm 0.005\\ 0.916 \pm 0.006\\ 0.928 \pm 0.006\\ 0.928 \pm 0.006\end{array}$	$\begin{array}{c} 0.964 \pm 0.004 \\ 0.970 \pm 0.004 \\ 0.966 \pm 0.005 \\ 0.966 \pm 0.005 \\ 0.969 \pm 0.005 \\ 0.948 \pm 0.005 \\ 0.948 \pm 0.005 \\ 0.958 \pm 0.005 \\ 0.960 \pm 0.005 \\ 0.960 \pm 0.005 \\ 0.962 \pm 0.005 \\ 0.962 \pm 0.005 \\ 0.928 \pm 0.006 \\ 0.922 \pm 0.006 \end{array}$	$\begin{array}{c} 0.965 \pm 0.00;\\ 0.945 \pm 0.00;\\ 0.941 \pm 0.00;\\ 0.955 \pm 0.00;\\ 0.965 \pm 0.00;\\ 0.964 \pm 0.00;\\ 0.964 \pm 0.00;\\ 0.922 \pm 0.00;\\ 0.925 \pm 0.00;\\$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	49.5 50.0 51.5 52.5 53.5 54.5 55.5 56.5 57.5 58.5 59.5 60.5 60.5 61.5	$\begin{array}{c} 0.960 \pm 0.004\\ 0.966 \pm 0.005\\ 0.963 \pm 0.005\\ 0.955 \pm 0.005\\ 0.955 \pm 0.005\\ 0.937 \pm 0.005\\ 0.952 \pm 0.005\\ 0.969 \pm 0.005\\ 0.960 \pm 0.005\\ 0.966 \pm 0.005\\ 0.916 \pm 0.006\\ 0.928 \pm 0.006\\$	$\begin{array}{c} 0.970\pm 0.004\\ 0.964\pm 0.005\\ 0.966\pm 0.005\\ 0.969\pm 0.005\\ 0.948\pm 0.005\\ 0.948\pm 0.005\\ 0.958\pm 0.005\\ 0.960\pm 0.005\\ 0.962\pm 0.005\\ 0.962\pm 0.005\\ 0.928\pm 0.006\\ 0.922\pm 0.006\end{array}$	$\begin{array}{c} 0.965 \pm 0.00;\\ 0.965 \pm 0.00;\\ 0.965 \pm 0.00;\\ 0.945 \pm 0.00;\\ 0.945 \pm 0.00;\\ 0.945 \pm 0.00;\\ 0.955 \pm 0.00;\\ 0.965 \pm 0.00;\\ 0.964 \pm 0.00;\\ 0.964 \pm 0.00;\\ 0.922 \pm 0.00;\\ 0.925 \pm 0.00;\\$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{ccccccc} 4 & 0.964 \pm 0.004 \\ 4 & 0.964 \pm 0.006 \\ 4 & 0.963 \pm 0.001 \\ 4 & 0.963 \pm 0.003 \\ 4 & 0.955 \pm 0.005 \\ 4 & 0.955 \pm 0.005 \\ 4 & 0.968 \pm 0.004 \\ 4 & 0.972 \pm 0.003 \\ 3 & 0.966 \pm 0.001 \\ 3 & 0.965 \pm 0.003 \\ 3 & 0.965 \pm 0.005 \\ 3 & 0.961 \pm 0.003 \\ 3 & 0.961 \pm 0.003 \end{array}$	50.0 51.5 52.5 53.5 54.5 55.5 56.5 57.5 58.5 59.5 60.5 60.5 61.5	$\begin{array}{c} 0.965 \pm 0.005\\ 0.963 \pm 0.005\\ 0.955 \pm 0.005\\ 0.942 \pm 0.005\\ 0.937 \pm 0.005\\ 0.952 \pm 0.005\\ 0.969 \pm 0.005\\ 0.969 \pm 0.005\\ 0.966 \pm 0.005\\ 0.916 \pm 0.006\\ 0.928 \pm 0.006\\ 0.928 \pm 0.006\end{array}$	$\begin{array}{c} 0.964 \pm 0.005 \\ 0.966 \pm 0.005 \\ 0.969 \pm 0.005 \\ 0.948 \pm 0.005 \\ 0.944 \pm 0.005 \\ 0.958 \pm 0.005 \\ 0.960 \pm 0.005 \\ 0.967 \pm 0.005 \\ 0.962 \pm 0.005 \\ 0.928 \pm 0.006 \\ 0.922 \pm 0.006 \end{array}$	$\begin{array}{c} 0.965 {\pm} 0.00;\\ 0.965 {\pm} 0.00;\\ 0.965 {\pm} 0.00;\\ 0.945 {\pm} 0.00;\\ 0.945 {\pm} 0.00;\\ 0.955 {\pm} 0.00;\\ 0.965 {\pm} 0.00;\\ 0.964 {\pm} 0.00;\\ 0.964 {\pm} 0.00;\\ 0.922 {\pm} 0.00;\\ 0.925 {\pm} 0.00;\\$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{ccccccc} 4 & 0.964\pm 0.006\\ 4 & 0.963\pm 0.001\\ 4 & 0.963\pm 0.003\\ 4 & 0.955\pm 0.005\\ 4 & 0.968\pm 0.004\\ 4 & 0.972\pm 0.003\\ 3 & 0.966\pm 0.003\\ 3 & 0.965\pm 0.003\\ 3 & 0.965\pm 0.005\\ 3 & 0.961\pm 0.003\\ 3 & 0.961\pm 0.003\\ \end{array}$	51.5 52.5 53.5 54.5 55.5 56.5 57.5 58.5 59.5 60.5 61.5	$\begin{array}{c} 0.963 \pm 0.005\\ 0.955 \pm 0.005\\ 0.942 \pm 0.005\\ 0.937 \pm 0.005\\ 0.952 \pm 0.005\\ 0.969 \pm 0.005\\ 0.960 \pm 0.005\\ 0.966 \pm 0.005\\ 0.916 \pm 0.006\\ 0.928 \pm 0.006\\ 0.928 \pm 0.006\end{array}$	$\begin{array}{c} 0.966 \pm 0.005 \\ 0.969 \pm 0.005 \\ 0.948 \pm 0.005 \\ 0.944 \pm 0.005 \\ 0.958 \pm 0.005 \\ 0.960 \pm 0.005 \\ 0.967 \pm 0.005 \\ 0.962 \pm 0.005 \\ 0.928 \pm 0.006 \\ 0.922 \pm 0.006 \end{array}$	$\begin{array}{c} 0.965 {\pm} 0.001 \\ 0.962 {\pm} 0.001 \\ 0.945 {\pm} 0.002 \\ 0.945 {\pm} 0.002 \\ 0.945 {\pm} 0.002 \\ 0.955 {\pm} 0.002 \\ 0.965 {\pm} 0.004 \\ 0.964 {\pm} 0.002 \\ 0.964 {\pm} 0.002 \\ 0.922 {\pm} 0.006 \\ 0.925 {\pm} 0.003 \end{array}$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{ccccccc} 4 & 0.963 \pm 0.001 \\ 4 & 0.963 \pm 0.003 \\ 4 & 0.955 \pm 0.005 \\ 4 & 0.968 \pm 0.004 \\ 4 & 0.972 \pm 0.003 \\ 3 & 0.966 \pm 0.001 \\ 3 & 0.965 \pm 0.003 \\ 3 & 0.965 \pm 0.003 \\ 3 & 0.965 \pm 0.005 \\ 3 & 0.961 \pm 0.003 \\ 3 & 0.961 \pm 0$	52.5 53.5 54.5 55.5 56.5 57.5 58.5 59.5 60.5 61.5	$\begin{array}{c} 0.955\pm 0.005\\ 0.942\pm 0.005\\ 0.937\pm 0.005\\ 0.952\pm 0.005\\ 0.969\pm 0.005\\ 0.960\pm 0.005\\ 0.966\pm 0.005\\ 0.916\pm 0.006\\ 0.928\pm 0.$	$\begin{array}{c} 0.369\pm 0.005\\ 0.948\pm 0.005\\ 0.944\pm 0.005\\ 0.958\pm 0.005\\ 0.960\pm 0.005\\ 0.967\pm 0.005\\ 0.962\pm 0.005\\ 0.928\pm 0.006\\ 0.922\pm 0.006\\ \end{array}$	$\begin{array}{c} 0.962\pm 0.00\\ 0.945\pm 0.00\\ 0.945\pm 0.00\\ 0.955\pm 0.00\\ 0.965\pm 0.00\\ 0.964\pm 0.00\\ 0.964\pm 0.00\\ 0.922\pm 0.00\\ 0.925\pm 0.00\\ \end{array}$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	53.5 54.5 55.5 56.5 57.5 58.5 59.5 60.5 61.5	$\begin{array}{c} 0.942\pm 0.005\\ 0.937\pm 0.005\\ 0.952\pm 0.005\\ 0.969\pm 0.005\\ 0.960\pm 0.005\\ 0.966\pm 0.005\\ 0.916\pm 0.006\\ 0.928\pm 0.006\\ 0.928\pm 0.006\end{array}$	$\begin{array}{c} 0.948 \pm 0.005 \\ 0.944 \pm 0.005 \\ 0.958 \pm 0.005 \\ 0.960 \pm 0.005 \\ 0.967 \pm 0.005 \\ 0.962 \pm 0.005 \\ 0.928 \pm 0.006 \\ 0.922 \pm 0.006 \end{array}$	$\begin{array}{c} 0.945 {\pm} 0.00;\\ 0.941 {\pm} 0.00;\\ 0.955 {\pm} 0.00;\\ 0.965 {\pm} 0.00;\\ 0.964 {\pm} 0.00;\\ 0.964 {\pm} 0.00;\\ 0.922 {\pm} 0.00;\\ 0.925 {\pm} 0.00;\\$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	54.5 55.5 56.5 57.5 58.5 59.5 60.5 61.5	$\begin{array}{c} 0.937 \pm 0.005\\ 0.952 \pm 0.005\\ 0.969 \pm 0.005\\ 0.960 \pm 0.005\\ 0.966 \pm 0.005\\ 0.916 \pm 0.006\\ 0.928 \pm 0.006\\ 0.928 \pm 0.006\end{array}$	$\begin{array}{c} 0.944 \pm 0.005 \\ 0.958 \pm 0.005 \\ 0.960 \pm 0.005 \\ 0.967 \pm 0.005 \\ 0.962 \pm 0.005 \\ 0.928 \pm 0.006 \\ 0.922 \pm 0.006 \end{array}$	$\begin{array}{c} 0.941 {\pm} 0.00, \\ 0.955 {\pm} 0.00, \\ 0.965 {\pm} 0.00, \\ 0.964 {\pm} 0.00, \\ 0.964 {\pm} 0.00, \\ 0.922 {\pm} 0.00, \\ 0.925 {\pm} 0.00, \end{array}$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{ccccccc} 4 & 0.968 \pm 0.004 \\ 4 & 0.972 \pm 0.003 \\ 3 & 0.966 \pm 0.001 \\ 3 & 0.965 \pm 0.003 \\ 3 & 0.965 \pm 0.003 \\ 3 & 0.965 \pm 0.005 \\ 3 & 0.961 \pm 0.003 \\ 3 & 0.961 \pm 0.003 \end{array}$	55.5 56.5 57.5 58.5 59.5 60.5 61.5	$\begin{array}{c} 0.952\pm0.005\\ 0.969\pm0.005\\ 0.960\pm0.005\\ 0.966\pm0.005\\ 0.916\pm0.006\\ 0.928\pm0.006\\ 0.928\pm0.006$	$\begin{array}{c} 0.958 {\pm} 0.005 \\ 0.960 {\pm} 0.005 \\ 0.967 {\pm} 0.005 \\ 0.962 {\pm} 0.005 \\ 0.928 {\pm} 0.006 \\ 0.922 {\pm} 0.006 \end{array}$	$\begin{array}{c} 0.955 \pm 0.00;\\ 0.965 \pm 0.00;\\ 0.964 \pm 0.00;\\ 0.964 \pm 0.00;\\ 0.922 \pm 0.00;\\ 0.922 \pm 0.00;\\ 0.925 \pm 0.00;\\ \end{array}$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{ccccccc} 4 & 0.972\pm0.003 \\ 3 & 0.966\pm0.001 \\ 3 & 0.964\pm0.003 \\ 3 & 0.965\pm0.003 \\ 3 & 0.965\pm0.005 \\ 3 & 0.961\pm0.005 \\ 3 & 0.961\pm0.003 \end{array}$	56.5 57.5 58.5 59.5 60.5 61.5	$\begin{array}{c} 0.969 \pm 0.005 \\ 0.960 \pm 0.005 \\ 0.966 \pm 0.005 \\ 0.916 \pm 0.006 \\ 0.928 \pm 0.006 \end{array}$	$\begin{array}{c} 0.960 \pm 0.005 \\ 0.967 \pm 0.005 \\ 0.962 \pm 0.005 \\ 0.928 \pm 0.006 \\ 0.922 \pm 0.006 \end{array}$	$\begin{array}{c} 0.965 \pm 0.004 \\ 0.964 \pm 0.003 \\ 0.964 \pm 0.004 \\ 0.922 \pm 0.006 \\ 0.925 \pm 0.003 \end{array}$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	57.5 58.5 59.5 60.5 61.5	$\begin{array}{c} 0.960 \pm 0.005 \\ 0.966 \pm 0.005 \\ 0.916 \pm 0.006 \\ 0.928 \pm 0.006 \end{array}$	$\begin{array}{c} 0.967 \pm 0.005 \\ 0.962 \pm 0.005 \\ 0.928 \pm 0.006 \\ 0.922 \pm 0.006 \end{array}$	$\begin{array}{c} 0.964 \pm 0.00; \\ 0.964 \pm 0.004 \\ 0.922 \pm 0.006 \\ 0.925 \pm 0.003 \end{array}$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccc} 3 & 0.964 \pm 0.003 \\ 3 & 0.965 \pm 0.003 \\ 3 & 0.965 \pm 0.005 \\ 3 & 0.961 \pm 0.003 \end{array}$	58.5 59.5 60.5 61.5	$\begin{array}{c} 0.966 {\pm} 0.005 \\ 0.916 {\pm} 0.006 \\ 0.928 {\pm} 0.006 \end{array}$	$\begin{array}{c} 0.962 {\pm} 0.005 \\ 0.928 {\pm} 0.006 \\ 0.922 {\pm} 0.006 \end{array}$	0.964 ± 0.004 0.922 ± 0.006 0.925 ± 0.003
$\begin{array}{ccccccc} 7\pm 0.003 & & 0.962\pm 0.003 \\ 0\pm 0.003 & & 0.961\pm 0.003 \\ 8\pm 0.003 & & 0.964\pm 0.003 \\ 5\pm 0.003 & & 0.966\pm 0.003 \end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	59.5 60.5 61.5	0.916 ± 0.006 0.928 ± 0.006	0.928 ± 0.006 0.922 ± 0.006	0.922 ± 0.006 0.925 ± 0.003
$\begin{array}{ccccccc} 0\pm 0.003 & 0.961\pm 0.003 \\ 8\pm 0.003 & 0.964\pm 0.003 \\ 5\pm 0.003 & 0.966\pm 0.003 \end{array}$	$\begin{array}{ccc} 3 & 0.965 \pm 0.005 \\ 0.961 \pm 0.003 \\ \end{array}$	60.5 61.5	0.928 ± 0.006	0.922 ± 0.006	0.925 ± 0.003
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.961 ± 0.003	61.5	0 0 0 0 0 0 0 0 0 0		
5 ± 0.003 0.966±0.003	0 0 0 0 0 0 0 0		0.955 ± 0.006	0.948 ± 0.006	0.952 ± 0.004
	0.970 ± 0.004	62.5	0.980 ± 0.006	0.972 ± 0.006	0.976 ± 0.004
8 ± 0.003 0.964 ±0.003	0.961 ± 0.003	63.5	0.956 ± 0.006	0.967 ± 0.006	0.962 ± 0.005
4 ± 0.003 0.967 ±0.003	0.971 ± 0.004	64.5	0.935 ± 0.006	0.926 ± 0.006	0.931 ± 0.005
8 ± 0.003 0.963 ± 0.004	4 0.971 ± 0.004	65.5	0.915 ± 0.005	0.926 ± 0.005	0.920 ± 0.006
8 ± 0.005 0.958 ±0.003	0.963 ± 0.005	66.5	0.932 ± 0.005	0.932 ± 0.005	0.932 ± 0.006
4 ± 0.005 0.963 ± 0.003	0.964 ± 0.001	67.5	0.945 ± 0.005	0.934 ± 0.005	0.940 ± 0.006
3 ± 0.005 0.960 ± 0.003	0.962 ± 0.002	68.5	0.958 ± 0.005	0.964 ± 0.005	0.961 ± 0.003
7 ± 0.005 0.961 ±0.003	0.964 ± 0.003	69.5	0.978 ± 0.005	0.977 ± 0.005	0.978 ± 0.001
6 ± 0.005 0.964 ± 0.003	0.965 ± 0.001	70.5	0.957 ± 0.006	0.964 ± 0.006	0.960 ± 0.004
5 ± 0.004 0.966±0.004	0.966 ± 0.001	71.5	0.928 ± 0.006	0.922 ± 0.006	0.925 ± 0.003
6 ± 0.004 0.962 ± 0.004	4 0.964 + 0.002	72.5	0.920 ± 0.006	0.912 ± 0.006	0.916 ± 0.004
0 ± 0.004 0.968 ± 0.004	$4 0.965 \pm 0.004$	73.5	0.922 ± 0.006	0.917 ± 0.006	0.920 ± 0.003
8 ± 0.004 0.963 ±0.004	0.966 ± 0.003	74.5	0.938 ± 0.006	0.928 ± 0.006	0.933 ± 0.003
5 ± 0.004 0.962 ±0.004	$4 0.963 \pm 0.002$		-	an fax	
2 ± 0.005 0.969 ± 0.005	0.971 ± 0.002				
4376560852	$\begin{array}{cccccccc} \pm 0.005 & 0.963 \pm 0.005 \\ \pm 0.005 & 0.960 \pm 0.005 \\ \pm 0.005 & 0.961 \pm 0.005 \\ \pm 0.005 & 0.964 \pm 0.005 \\ \pm 0.004 & 0.966 \pm 0.00 \\ \pm 0.004 & 0.962 \pm 0.00 \\ \pm 0.004 & 0.963 \pm 0.00 \\ \pm 0.004 & 0.963 \pm 0.00 \\ \pm 0.004 & 0.962 \pm 0.00 \\ \pm 0.004 & 0.962 \pm 0.00 \\ \pm 0.004 & 0.962 \pm 0.00 \\ \pm 0.005 & 0.969 \pm 0.003 \\ \end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$

Table 2 (a).—Measured Activation Energies (E/R)/1000 for n- Octane in the Temperature Range of 5°C. to 75°C. Using $\Delta T = 1°C$.

TAYEB M. QURESHI, S.A. BARI AND M. M. QURASHI



Fig. 2.—Plot of variation of (E/R)/1000 with temperature obtained with the improved technique at intervals of 1°C. for n-octane. Upper graph (hollow circles) is for n-octane from 5°C. to 75°C. A long flat extending over at least 45°C. changes over to cyclic variation at 52°C. \mp 2°C.

Lower graph (solid circles) is for iso-octane, showing anomalous behaviour, viz. cyclic variation of E/R at lower temperatures, going over to constant value of E/R at 54°C. This straight line goes to a considerable range, close to its boiling point (99.2°C.).

especial care had to be taken during viscosity measurements in the range of 4°C. to 50°C. at thermal interval of 1°C. Particular care was necessary in sucking the liquid up in the capillary limb bulb. The flow times in seconds (measured in viscometer No. 'O' and corrected for equilibrium level), the Beckmann readings, the mean temperature (°C.) and the calculated values of (E/R)/1000, together with r.m.s. deviations as estimated for the successive sets of five readings taken at a stretch (which is of the order of ± 0.004 units of E/R - 1000) are given in Table 3 for both the heating and cooling sequences. Fig. 3, plotted to the same scale as for n-octane, etc., is the graphical representation of these (E/R)/1000 values (hollow circles), where the radii of these circles are approximately of the magnitude of r.m.s. deviations. This curve shows clear normal steplike variation upto $38^{\circ}C. \mp 2^{\circ}C.$, the average step-length being $15^{\circ}C.$ The two sharp jumps at 24.5°C., which are of the magnitude of 0.05 and 0.04 units of (E/R)/1000 respectively, viz. twelve and ten times the r.m.s. error, are quite significant. Above this temperature of $38^{\circ}C.\mp 2^{\circ}C.$, the phenomena undergo the usual change in E, and the energy begins to oscillate with a cycle of $8.2^{\circ}C.$ and peak-to-peak amplitude of 0.07 units of (E/R)/1000, which is seven times the r.m.s. deviations.

Results on Kerosene Oil and Discussion

Thus, it is evident that all the straight-chain, hydrocarbons so far investigated exhibit a steplike variation of a definite pattern at the lower temperatures, and undergo abrupt change to cyclic variation of definite amplitude and period at higher temperatures, well below the boiling point. This transition temperature is apparently a characteristic of various factors, among which

Mean	(E/	$R)/1000 = -T^2(\Delta \ln \upsilon/\Delta$	T)/1000	Mean	$(E/R)/1000 = -T^2 (\Delta \ln \upsilon / \Delta T)/1000$				
rature (°C.)	Heating sequence	Cooling sequence	Mean	rature (°C.)	Heating sequence	Cooling sequence	Mean		
5.5	0.930 ± 0.003	0.935 ± 0.003	0.932+0.003	40.5	0.910+0.004	0.904 ± 0.004	0.907+0.003		
6.5	0.917 ± 0.003	0.924 ± 0.003	0.920 ± 0.004	41.5	0.898 ± 0.004	0.904 ± 0.004	0.901 ± 0.003		
7.5	0.920 ± 0.003	0.928 ± 0.003	0.924 ± 0.004	42.5	0.924 ± 0.004	0.914 ± 0.004	0.919 ± 0.005		
8.5	0.905 ± 0.003	0.894 ± 0.003	0.899 ± 0.005	43.5	0.925 ± 0.004	0.920 ± 0.004	0.923 ± 0.003		
9.5	0.896 ± 0.003	0.990 ± 0.003	0.893 ± 0.003	44.5	0.932 ± 0.004	0.927 ± 0.004	0.930 ± 0.003		
10.5	0.920 ± 0.004	0.916 ± 0.004	0.918 ± 0.002	45.5	0.920 ± 0.005	0.925 ± 0.005	0.922 ± 0.003		
11.5	0.922 ± 0.004	0.932 ± 0.004	0.927 ± 0.004	46.5	0.887 ± 0.005	0.896 ± 0.005	0.892 ± 0.004		
12.5	0.900 ± 0.004	0.908 ± 0.004	0.904 ± 0.004	47.5	0.900 ± 0.005	0.891 ± 0.005	0.895 ± 0.004		
13.5	0.900 ± 0.004	0.893 ± 0.004	0.896 ± 0.003	48.5	0.912 ± 0.005	0.903 ± 0.005	0.907 ± 0.005		
14.5	0.905 ± 0.004	0.917 ± 0.004	0.911 ± 0.004	49.5	0.932 ± 0.005	0.924 ± 0.005	0.928 ± 0.004		
15.5	0.918 ± 0.003	0.923 ± 0.003	0.920 ± 0.002	50.5	0.933 ± 0.003	0.944 ± 0.003	0.938 ± 0.006		
6.5	0.942 ± 0.003	0.952 ± 0.003	0.947 ± 0.004	51.5	0.930 ± 0.003	0.918 ± 0.003	0.924 ± 0.006		
7.5	0.956 ± 0.003	0.949 ± 0.003	0.953 ± 0.004	52.5	0.890 ± 0.003	0.897 ± 0.003	0.893 ± 0.004		
8.5	0.960 ± 0.003	0.945 ± 0.003	0.952 ± 0.007	53.5	0.900 ± 0.003	0.901 ± 0.003	0.901 ± 0.001		
9.5	0.925 ± 0.003	0.922 ± 0.003	0.923 ± 0.002	54.5	0.955 ± 0.003	0.947 ± 0.003	0.951 ± 0.005		
20.5	0.895 ± 0.005	0.905 ± 0.005	0.900 ± 0.005	55.5	0.953 ± 0.003	0.954 ± 0.003	0.954 ± 0.001		
21.5	0.910 ± 0.005	0.901 ± 0.005	0.905 ± 0.005	56.5	0.953 ± 0.003	0.943 ± 0.003	0.948 ± 0.005		
22.5	0.898 ± 0.005	0.898 ± 0.005	0.898 ± 0.000	57.5	0.953 ± 0.003	0.945 ± 0.003	0.949 + 0.004		
23.5	0.918 ± 0.005	0.908 ± 0.005	0.913 ± 0.005	58.5	0.956 ± 0.003	0.946 ± 0.003	0.951 ± 0.005		
4.5	0.919 ± 0.005	0.911 ± 0.005	0.915 ± 0.004	59.5	0.958 ± 0.003	0.950 ± 0.003	0.954 ± 0.004		
5.5	0.895 ± 0.004	0.887 ± 0.004	0.891 ± 0.004	60.5	0.944 ± 0.005	0.950 ± 0.005	0.947 ± 0.003		
6.5	0.868 ± 0.004	0.862 ± 0.004	0.865 ± 0.003	61.5	0.948 ± 0.005	0.955 ± 0.005	0.951 ± 0.004		
27.5	0.864 ± 0.004	0.878 ± 0.004	0.871 ± 0.007	62.5	0.960 ± 0.005	0.942 ± 0.005	0.951 ± 0.009		
8.5	0.875 ± 0.004	0.877 ± 0.004	0.876 ± 0.001	63.5	0.952 ± 0.005	0.952 ± 0.005	0.952 ± 0.000		
9.5	0.902 ± 0.004	0.894 ± 0.004	0.898 ± 0.004	64.5	0.956 ± 0.005	0.950 ± 0.005	0.953 ± 0.003		
0.5	0.914 ± 0.003	0.907 ± 0.003	0.911 ± 0.004	65.5	0.952 ± 0.004	0.959 ± 0.004	0.955 ± 0.004		
1.5	0.907 ± 0.003	0.900 ± 0.003	0.903 ± 0.003	66.5	0.946 ± 0.004	0.950 ± 0.004	0.948 ± 0.002		
2.5	0.886 ± 0.003	0.894 ± 0.003	0.890 ± 0.006	67.5	0.957 ± 0.004	0.953 ± 0.004	0.955 ± 0.002		
3.5	0.886 + 0.003	0.893 ± 0.003	0.889 ± 0.004	68.5	0.950 ± 0.004	0.945 ± 0.004	0.948 ± 0.003		
4.5	0.896 ± 0.003	0.900 ± 0.003	0.898 ± 0.002	67.5	0.955 ± 0.004	0.948 ± 0.004	0.951 ± 0.003		
5.5	0.906 ± 0.004	0.895 ± 0.004	0.901 ± 0.004	68.5	0.958 ± 0.005	0.943 ± 0.005	0.951 ± 0.008		
6.5	0.912 ± 0.004	0.907 + 0.004	0.909 ± 0.002	69.5	0.953 ± 0.005	0.950 ± 0.005	0.951 ± 0.001		
57.5	0.925 ± 0.004	0.922 ± 0.004	0.923 ± 0.003	70.5	0.950 ± 0.005	0.956 ± 0.005	0.953 ± 0.003		
38.5	0.930 ± 0.004	0.921 ± 0.004	0.925 ± 0.004	71.5	0.959 ± 0.005	0.950 ± 0.005	0.954 ± 0.005		
norme (CC)	The second s			72.5	0.955 ± 0.005	0.954 ± 0.005	0.955 ± 0.001		

TABLE 2 (b).—MEASURED	ACTIVATION	Energies	$E/R \div$	1000 FOR	ISO-OCTANE	(2:2:4	TRIMETHYL				
Pentane) in the Range of 5° to 73°C. Using $\Delta T = 1°C$.											

Heating sequence									Cool	ing sequ	ence		
Te	em-	Beckmann	Time of flow	Mean	E/1	R÷1000	Tem-	Backmann	Time of flow	Mean	E/F	₹÷1000	Overall
tu (°	re C.)	reading	ected for level	rature (°C.)	Unco- rrected	Corrected	ture (°C.)	reading	corrected for level	rature (°C.)	Unco- rrected	Corrected	(E/R)/1000
	1	2	3	4	5	6	7	8	9	10	11	12	13
4	.0 1	$.356 \pm 0.001$	761.87 ± 0.02		0.040	0.051.0.001	4.0	1.360 ± 0.000	761.88 ± 0.02			0.044.0.004	0.054.0.005
5	.0 2	2.352 ± 0.000	753.57±0.02	4.50	0.848	0.851±0.004	5.0	2.362 ± 0.001	753.43 ± 0.03	4.50	0.758	0.861 ± 0.004	0.856 ± 0.005
6	.0 3	3.358 ± 0.001	745.38 ± 0.03	5.50	0.847	0.843 ± 0.004	6.0	3.360 ± 0.000	745.35 ± 0.00	5.50	0.839	0.835 ± 0.004	0.839 ± 0.004
6	.0 0	0.080 ± 0.001	745.36±0.02	< F0	0.064	0.0(1.).0.000	6.0	0.080±0.000	$745.36{\pm}0.01$	6.60	0.057	0.057 . 0.000	0.050 + 0.000
7	.0 1	1.080 ± 0.000	737.22 ± 0.02	6.50	0.861	0.861 ± 0.002	7.0	1.083 ± 0.000	737.21±0.02	6.60	0.857	0.857±0.002	0.859 ± 0.002
8	.0 2	2.090 ± 0.001	729.91±0.03	7.50	0.778	0.778±0.002	8.0	2.095 ± 0.000	729.80 ± 0.02	7.50	0.786	0.786 ± 0.002	0.782 ± 0.004
9	.0 3	3.090 ± 0.000	722.77 ± 0.01	8.50	0.781	0.780±0.002	9.0	3.090 ± 0.000	722.61 ± 0.01	8.50	0.790	0.789 ± 0.002	0.785 ± 0.005
10	.0 4	4.110 ± 0.001	715.54 ± 0.01	9.50	0.784	0.786±0.002	10.0	4.118 ± 0.001	715.44 ± 0.02	9.50	0.775	0.774 ± 0.002	0.780 ± 0.008
11	.0 5	5.133 ± 0.000	708.44±0.00	10.50	0,784	0.780 ± 0.002	11.0	5.136 ± 0.001	708.39 ± 0.02	10.50	0.781	0.785 ± 0.002	0.784 ± 0.001
. 11	.0 0	0.008 ± 0.000	711.24±0.01	11 50	0 505		11.0	0.010 ± 0.001	711.27±0.02	44 50	0.505		0. 500 + 0. 000
12	.0 0	0.980 ± 0.001	704.47 ± 0.03	11.50	0.785	0.782 ± 0.003	12.0	0.983 ± 0.002	704.46 ± 0.00	11.50	0.785	0.782 ± 0.003	0.782 ± 0.000
13	.0 1	$.960 \pm 0.000$	697.90±0.01	12.50	0.780	0.780±0.003	13.0	1.960 ± 0.000	697.83±0.02	12.50	0.790	0.790±0.003	0.785 ± 0.005
14	.0 2	2.981 ± 0.001	691.10±0.02	13.50	0.788	0.784 ± 0.003	14.0	2.986 ± 0.000	690.96±0.01	13.50	0.792	0.788 ± 0.003	0.786 ± 0.002
15	.0 3	3.971 ± 0.000	684.63±0.02	15.60	0.700	0.790 ± 0.003	15.0	3.967 ± 0.000	684.60±0.02	14.50	0.780	0.784 ± 0.003	0.787 ± 0.003
16	.0 4	$.989 \pm 0.001$	678.14±0.03	15.00	0.780	0.785±0.005	16.0	4.993±0.000	678.09±0.01	15.50	0.770	0.779±0.003	0.781 ± 0.002
16.	.0 0	0.063 ± 0.000	677.90±0.01	16 50	0.700	0 707 1 0 000	16.0	0.063 ± 0.000	677.89 ± 0.00	44 50	0.707	0.704 + 0.000	0 700 1 0 007
17.	.0 1	$.069 \pm 0.000$	671.51±0.02	10.50	0.790	0.787±0.002	17.0	1.073 ± 0.001	671.42±0.02	10.50	0.797	0.794±0.002	0.790 ± 0.003
18	.0 2	2.081 ± 0.001	665.10 ± 0.02	18.50	0.800	0.800±0.002	18.0	2.078 ± 0.000	665.11±0.02	19 50	0.794	0.794 ± 0.002	0.797 ±0.003
19	.0 3	0.060 ± 0.000	658.97±0.02	10.50	0.004	0.000 ± 0.002	19.0	3.060 ± 0.000	659.06±0.02	16.50	0,791	0.787 ± 0.002	0.793 ± 0.000
18,	,0 2	2.085 ± 0.000	666.49±0.02				18.0	2.085 ± 0.000	666.56±0.00				

TABLE 3.—BECKMANN READINGS, MEAN TEMPERATURES IN °C., FLOW TIMES AND THE CALCULATED VALUES OF $(E/R)/1000 = -T^2 (\Delta \ln \nu/\Delta T)/1000$ for n-Hexane from 5°C. to 50°C. Using Viscometer No '0' and $\Delta T = 1°C$.

(Continued) :---

(Table 3 Continued)

1	2	3	4	5	6	. 7	8	9	10	11	12	13
19.0	3 076±0 001	660 35 + 0 03	18.50	0.794	0.790 ± 0.003	19 0	3 072+0 001	660 49±0 02	18.50	0.789	0.784 ± 0.003	0.787 ± 0.003
20.0	1.075 ± 0.000	654.29 ± 0.01	19.50	0.790	$0.794 {\pm} 0.003$	20.0	4.080±0.000	654.33 ± 0.01	19.50	0.796	0.800 ± 0.003	0.797 ± 0.003
20.0	4.073±0.000	$(49, 29 \pm 0.01)$	20.50	0.790	0.793 ± 0.003	20.0	5.080±0.001	649 33 LO 02	20.50	00.794	0.797 ± 0.003	0.795 ± 0.002
21.0	5.082±0.000	648.28±0.02				21.0	5.080±0.001	040.33±0.02				
21.0	0.363 ± 0.001	648.06 ± 0.02	21.50	0.796	0.801 ± 0.004	21.0	0.365 ± 0.000	648.15±0.02	21.50	0.781	0.786 ± 0.004	0.793 ± 0.007
22.0	1.355 ± 0.000	642.19±0.01	22.50	0.800	0.795 ± 0.004	22,0	1.362 ± 0.000	642.37 ± 0.01	22.50	0.803	0.798 ± 0.004	0.796 ± 0.002
23.0	2.402 ± 0.001	636.06 ± 0.01	23.50	0.787	$0.785 {\pm} 0.004$	23.0	2.406 ± 0.001	636.26 ± 0.02	23.50	0.800	0.798 ± 0.004	0.791 ± 0.007
24.0	3.410 ± 0.000	630.35 ± 0.02	24.50	0.744	$0.750 {\pm} 0.004$	24.0	3.408 ± 0.000	630.49 ± 0.02	24.50	0.752	0.758 ± 0.004	0.754 ± 0.004
25.0	4.442±0.000	624.92 ± 0.01	25.50	0.737	0.732 ± 0.004	25.0	4.440 ± 0.001	624.99 ± 0.01	25.50	0.732	0.727 ± 0.004	0.730 ± 0.002
26.0	5.410 ± 0.001	619.94±0.02				26.0	5.410 ± 0.000	620.04 ± 0.01				
25.6	0.943±0.000	621.13±0.02	26.30	0.738	0.738 ± 0.003	26.0	0.985 ± 0.000	620.94±0.02	26.50	0 736	0.736 ± 0.003	0.737 ± 0.001
27.0	1.981 ± 0.000	615.85 ± 0.01	27.7	0.748	0.745 ± 0.003	27.0	1.980 ± 0.000	615.85±0.00	27.75	0.740	0.737 ± 0.003	0.741 ± 0.001
28.5	3.489 ± 0.001	608.23 ± 0.02	29.25	0.734	0.739 ± 0.003	28.5	3.484 ± 0.001	608.33±0.02	29.25	0.739	0.744 ± 0.003	0.741 ± 0.003
30.0	4.992 ± 0.000	600.92 ± 0.01	27.20	0.701	0.707_0.000	30.0	4.990±0.000	600.91±0.01	27.20	0.757	0.744_0.000	0.711_0.000
30.0	$0.091 {\pm} 0.001$	600.92 ± 0.02	30.50	0 725	0 728±0 003	30.0	$0.090 {\pm} 0.000$	$600.91 {\pm} 0.01$	30.50	0 737	0.740 ± 0.003	0.734 ± 0.006
31.0	1.100 ± 0.000	596.17 ± 0.01	31 50	0.725	0.748 ± 0.003	31.0	1.100 ± 0.001	596.78±0.03	31 50	0.743	0.740 ± 0.003	0.74 ± 0.004
32.0	2.122 ± 0.000	591.27±0.02	32.50	0.751	0.740 ± 0.003	32.0	2.120 ± 0.000	591.23 ± 0.01	32.50	0.745	0.741 ± 0.003	0.744 ± 0.004
33.0	3.100 ± 0.000	586.64 ± 0.01	32.50	0.731	0.741 ± 0.003	33.0	3.105 ± 0.000	586.59 ± 0.01	32.50	0.747	0.743 ± 0.003	0.745 ± 0.002
34.0	4.092 ± 0.001	582.09±0.02	24 50	0.735	0.741 ± 0.003	34.0	4.096±0.000	582.01 ± 0.02	33.50	0.745	0.749 ± 0.003	0.743 ± 0.004
55.0	5.083 ± 0.000	577.63 ± 0.02	34.30	0.755	0.737 ± 0.003	35.0	5.085 ± 0.000	577.53 ± 0.02	34.50	0.740	0.742 ± 0.003	0.739±0.002
35.0	-0.128 ± 0.000	576.60±0.01	25 50	0.740	0.750 1.0.002	35.0	-0.125±0.000	576.58 ± 0.02	25 50	0.746	0.747 1.0.002	0.749.1.0.000
36.0	$0.880 {\pm} 0.000$	572.05 ± 0.02	35.50	0.749	0.750 ± 0.003	36.0	0.878 ± 0.001	572.07 ± 0.01	35.50	0.746	0.747±0.003	0.748 ± 0.002
37.0	1.876±0.001	567.64±0.02	36.50	0.745	0.747±0.003	37.0	1.870±0.000	567.70±0.02	36.50	0.741	0.743±0.003	0.745 ± 0.002
			37.50	0.738	0.734 ± 0.003		0.000		37.50	0.739	0.735 ± 0.003	0.735 ± 0.001
38.0	2.861 ± 0.000	563.38 ± 0.01	38,50	0.722	0.722 ± 0.003	38.0	2.862 ± 0.000	563.46 ± 0.01	38.50	0.723	0.723 ± 0.003	0.723±0.000
											(Continued) :

TAYEB M. QURESHI, S.A. BARI AND M. M. QURASHI

(Table 3 Continued)

1	2	3	4	5	6	7	8	9	10	11	12	13
39.0	3.855 ± 0.000	559.23±0.02	39 50	0 704	0.702 ± 0.003	39.0	$3.855 {\pm} 0.001$	559.31 ± 0.02	39.50	0.706	0.704 ± 0.003	0.703 ± 0.001
40.0	4.832±0.001	555.31 ± 0.01	57.50	0.701	0.702 <u>1</u> 0.000	40.0	4.832±0.000	555.38 ± 0.02	0,000	0		
40.0	0.032 ± 0.000	555.23 ± 0.01	40.50	0 722	0.721+0.003	40.0	0.030 ± 0.000	555.17 ± 0.01	40.50	0.710	0.709 ± 0.003	0.715 ± 0.006
41.0	1.032 ± 0.000	551.17±0.02	41 50	0.740	0.740 0.003	41.0	1.036 ± 0.001	551.15±0.03	41 50	0.733	0 733 0.003	0.736 0.003
42.0	2.036 ± 0.001	547.05±0.03	42 50	0.781	0.777 ± 0.003	42.0	2.034 ± 0.000	547.09±0.01	42.50	0.770	0.766 ± 0.003	0.771 ± 0.004
43.0	3.034±0.000	542.79±0.01	43 50	0.762	0.766 ± 0.003	43.0	3.038 ± 0.001	542.86±0.02	43.50	0.747	0.751 ± 0.003	0.758 ± 0.007
44.0	4.025 ± 0.001	538.72±0.02	44 50	0.747	0.744 ± 0.003	44.0	4.030±0.000	538.86 ± 0.01	44.50	0.745	0.742 ± 0.003	0.743 ± 0.001
45.0	5.031 ± 0.000	534.74 ± 0.02	11.00	0.717	0.71120.000	45.0	5.030 ± 0.000	534.90±0.02	11100	01712		
45.0	0.113±0.001	532.08±0.02	45 50	0 722	0 725+0 003	45.0	0.110 ± 0.000	532.07±0.02	45 50	0.712	0.715 ± 0.003	0.720 ± 0.005
46.0	1.110 ± 0.000	528.32±0.02	46.50	0.724	0.723 ± 0.003	46.0	1.110 ± 0.000	528.35 ± 0.01	46.50	0.721	0.718 ± 0.003	0.720 ± 0.002
47.0	2.123 ± 0.000	524.54±0.01	47.50	0.704	0.721 ± 0.003	47.0	2.125 ± 0.000	524.58 ± 0.01	47.50	0.701	0.697 ± 0.003	0.699 ± 0.002
48.0	3.053 ± 0.000	521.11±0.01	48.50	0.704	0.710 ± 0.003	48.0	3.053 ± 0.000	521.27 <u>+</u> 0.00	48.50	0.710	0.714 ± 0.003	0.712 ± 0.002
49.0	4.058±0.001	517.55±0.02	49 50	0.713	0.716 ± 0.003	49.0	4.060±0.000	$517.68 {\pm} 0.01$	49 50	0.715	0.718 ± 0.003	0.717 ± 0.001
50.0	5.060 ± 0.000	514.01 ± 0.01	12.00	0.715	0.710_0.000	50.0	5.060 ± 0.000	514.14±0.02		0.710	5	

0.004



Fig. 3.—Graph showing the variation of E/R with temperature °C. for n-hexane in the region of 4°C. to 50°C. This again shows a regular series of sharp steps, followed by cyclic variation above $38^{\circ} \mp 2^{\circ}$ C. the carbon chain length appears to be a major factor.

In order to examine this idea, the transition temperature collected on the few hydrocarbons,





Fig. 4.—(Bottom) Plot of (E/R)/1000 against temperature for Kerosene Oil (Mol. wt: 165) in the temperature range of 10° to 47°C. (solid circles) and 47°C. to 106°C. (hollow circles). This curve also shows a step-wise behaviour which undergoes to cyclic variation above $94\mp2°$ C. like the other hydrocarbons.

are plotted as solid and hollow circles in Fig. 4(top) against the number 'n' of carbon atoms in the molecule. The circle can all be connected by a smooth curve as shown in the figure, but there is a rather large gap between decane and H.S. diesel oil with n=15, where the curve exhibits maximum curvature. Accordingly, activation energy measurements were carried out on Kerosene oil of molecular weight 165, corresponding approximately to $C_{12}H_{26}$, and the results are shown in Fig. 4 (bottom). It is seen that here again there is a sequence of constant region of E/R



Fig. 5.—Plot of temperature of transition from step-wise behaviour to cyclic variation, against \log_{10}^{n} n is the number of carbon atoms in the molecule.

The solid circles are the points for purc normal hydrocarbons, hollow circles are for the mineral oils and the triangle is an additional point for Kerosene oil.

Inclined crosses are the boiling points and horizontal crosses are the freezing points for some of the hydrocarbons. separated by sharp steps upto a temperature of $94^{\circ}\mp 2^{\circ}$ C., after which the oscillatory behaviour sets in. This transition temperature is plotted as a triangle in Fig. 4 (top), and is seen to fall on the previously drawn curve.

With a view to further developing the relationship between this transition temperature and the number 'n' of carbon atoms in the chain, this graph is replotted against \log_{10} n in Fig. 5. The points are now well-represented by a straight line through them, and for comparison, the upper and lower series of crosses show the succession of boiling and freezing points of the corresponding liquids and pure hydrocarbons.

It is now apparent that the straight line (or curve in Fig. 4 (a)) representing the transition temperatures divides the liquid range into two phases of some sort, with step-like transitions in E/R occurring below the line and cyclic variations above the line. Presumably this regular and consistent transition is connected with a type of order disorder phenomenon occurring in all the hydrocarbons.

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