TEMPERATURE DEPENDENCE OF THE INTERMOLECULAR ACTIVATION ENERGY FOR FLOW IN LIQUIDS AND SOLUTIONS

Part III.—Periodicity of Activation Energy in Pure Benzene

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As a sequel to the series of investigations leading to the discovery of jumps in the activation energy E_{T} for viscous flow of several hydroxylic liquids, it was considered worthwhile to undertake similar measurements on a few typical non-hydroxylic liquids. Some results for benzene are reported here, and a satisfactory degree of reproducibility has been obtained in working with two samples of pure benzene using a measuring interval $\Delta T = 1^{\circ}C$.

Evidence of a nearly cyclic variation with an approximate period of 5°C. has been obtained in the range of 26° to 46°C., the peak-to-peak amplitude of $(E_{7}/R)/1000$ being 0.1, corresponding to changes in E_{7} of about 200 cal.mole.

1. Introduction

In previous communications on this subject, it has been shown that, with the use of a sufficiently small thermal interval of $1^{-2} \circ^{\circ} C$, the activation energy measurements for several hydroxylic liquids¹,² and aqueous alcohol³ solutions show sharp, regularly-recurring jumps in activation energy, E_{η} . In an effort to throw further light on those phenomena, it was considered desirable to investigate the flow activation energy for some nonhydroxylic liquids such as the paraffin oils, benzene, etc. The present communication gives the results of some experiments carried out on benzene, which was previously found to exhibit an anomalous temperature variation⁴ of the activation energy of mixing ΔG_m in solutions of heptane.

The measuring technique is the same as used in the previously reported experiments on flow activation energy of ethylene glycol,² where temperature control to 0.002°C. was maintained and the viscometer system was protected by drying tubes on either side. Three to five readings of flow-time were taken at each temperature, and the temperature intervals were measured on a fifth-degree thermometer in the preliminary experiment, and on a calibrated Beckmann differential thermometer in the later experiments. Values of E/R were calculated from the usual equation,

$$\begin{array}{l} {\rm E\eta}/{\rm R} \ = \ \Delta \ \ln \eta / \Delta \ ({\rm I/T}) \ = - \ {\rm T}^2 \ \Delta \ \ln \eta / \Delta {\rm T} \\ = - \ {\rm T}^2 \ \Delta \ \ln \nu / \Delta {\rm T} - {\rm T}^2 \ \beta \end{array}$$

2. Preliminary Experiment

This experiment was of an exploratory character and therefore the measurements were taken from 30° C. to 50° C. at intervals of 2° C. The actual flow-times at the various temperatures are shown in Table 1, together with their standard deviations and the calculated values of E/R for the heating and cooling sequence. The overall means are given in the last column and these are seen to have an r.m.s. error of about 0.015, i.e. a little over 1%, which is quite satisfactory.

A plot of these results is shown in the lowest graph (triangles) of Fig. 1 marked Expt. I, and one can readily observe the two maxima at 33 °C. and 45°C., the maximum-to-minimum variation being about 0.1 unit, i.e. seven times the r.m.s. error. A third max. is also noticeable near 38°C.

3. Experiments Using the Beckmann Thermometer

The second set of experiments was carried out at every degree centigrade using a Beckmann thermometer, and the calculations of E/R were made with a one-degree C. interval so as to obtain higher resolution. The results obtained are given in Table 2, where the last column gives the standard deviations as estimated (for groups of five temperatures) from the differences between the results for the heating and cooling sequences. A plot of this data labelled Expt. II is shown in the lower half of Fig. 1 as solid circles. The best curve drawn through these brings out quite clearly the three maxima observed in the preliminary experiment, as well as a series of others at intervals of about 4 °C.

In an effort to obtain still more information about the character of these more or less cyclic variations in the activation energy, a third experiment was carried out, but the temperatures were selected in such a way that the plotted points would fall midway between the solid circles of Expt. II. The actual flow-times and Beckmann readings taken at various temperatures are recorded in Table 3, the other columns of which give the corresponding values of E/R calculated for TEMPERATURE DEPENDENCE OF THE INTERMOLECULAR ACTIVATION ENERGY. PART III

Heating sequence				Cooling squence				Overall
Тетр. (°С.)	Time of flow (sec.) corrected for level	Mean temp. (°C.)	E'/R÷1000	Temp. (°C.)	Time of flow corrected for level	Mean temp. (°C.)	E'/R÷1000	mean E/R ÷ 1000
30.73±0.01	868.40+0.10	31.36	1.14	30.73±0.01	868.30±0.08	31.36	1 12	1 13 1 0 01
$\begin{array}{r} 32.00 \pm 0.00 \\ 34.00 \pm 0.00 \\ 36.00 \pm 0.00 \end{array}$	$\begin{array}{r} 854.96 \pm 0.20 \\ 832.51 \pm 0.07 \\ 812.53 \pm 0.11 \end{array}$	33.00 35.00	1.24 1.15	$\begin{array}{c} 32.00 \pm 0.01 \\ 34.00 \pm 0.00 \\ 36.00 \pm 0.00 \end{array}$	$\begin{array}{r} 855.00 \pm 0.10 \\ 832.65 \pm 0.10 \\ 812.77 \pm 0.10 \end{array}$	33.00 35.00	1.12 1.24 1.14 1	1.13 ± 0.01 $1.24 \pm .000$ $1.14_5 \pm 0.00_5$
$\begin{array}{c} 36.00 \pm 0.00 \\ 38.00 \pm 0.00 \\ 40.00 \pm 0.00 \end{array}$	$\begin{array}{c} 812.49 \pm 0.05 \\ 793.84 \pm 0.10 \\ 775.82 \pm 0.12 \end{array}$	37.00 39.00	1.12 1.12	$\begin{array}{c} 36.00 \pm 0.01 \\ 38.00 \pm 0.00 \\ 40.00 \pm 0.00 \end{array}$	$\begin{array}{c} 812.54 \pm 0.08 \\ 793.89 \pm 0.12 \\ 775.40 \pm 0.06 \end{array}$	37.00 39.00	1.12 1.16	1.12 ± 0.00 1.14 ± 0.02
$\begin{array}{c} 40.00 \pm 0.01 \\ 42.00 \pm 0.01 \\ 44.00 \pm 0.00 \\ 46.00 \pm 0.00 \end{array}$	$774.92 \pm 0.08 \\ 758.42 \pm 0.05 \\ 741.79 \pm 0.10 \\ 725.60 \pm 0.10$	41.00 43.00 45.00	1.07 1.11 1.12	$\begin{array}{c} 40.00 \pm 0.00 \\ 42.00 \pm 0.00 \\ 44.00 \pm 0.01 \\ 46.00 \pm 0.00 \end{array}$	$774.94 \pm 0.05 \\ 758.44 \pm 0.11 \\ 741.72 \pm 0.10 \\ 725.10 \pm 0.10$	41.00 43.00 45.00	1.07 1.12 1.15 1	1.07 ± 0.00 1.115 ± 0.005 1.135 ± 0.015
$\begin{array}{c} 46.00 \pm 0.00 \\ 48.00 \pm 0.00 \\ 50.00 \pm 0.00 \end{array}$	$\begin{array}{c} 725.02 \pm 0.10 \\ 709.18 \pm 0.20 \\ 694.69 \pm 0.10 \end{array}$	47.00 49.00	1.13 1.07	$\begin{array}{c} 46.00 \pm 0.01 \\ 48.00 \pm 0.00 \\ 50.00 \pm 0.01 \end{array}$	$\begin{array}{c} 725.01 \pm 0.08 \\ 709.50 \pm 0.12 \\ 694.90 \pm 0.10 \end{array}$	47.00 49.00	1.11 1.08	1.12 ± 0.01 1.075 ± 0.005

Table 1.—Temperature, Time of Flow and Calculated Values of $E'/R \div 1000 = -T^2(\Delta \ln \nu / \Delta T)/1000$ FOR PURE BENZENE (ANALAR GRADE) USING $\Delta T = 2^{\circ}C$.



Fig. 1.—Series of graphs showing the results of repeated experiments on benzene to determine the values of $E/R = -T2 \Delta \ln \omega / \Delta T$ at various temperatures:

(i) Lowest curve (triangles) is a plot of the measurements made at intervals of 2°C. with a fifth-degree thermometer, showing two

(i) Second curve (solid circles) marked "Expt. II" gives the results of the next experiment, which was carried out from 8°C. to 46°C. (ii) Second curve (solid circles) marked "Expt. II" gives the results of the next experiment, which was carried out from 8°C. to 46°C. with a measuring interval $\Delta T = 1^{\circ}C$, and using a Beckmann differential thermometer. The peaks at 33°C and 45°C are again seen, and in addition several more at intervals of 4° to 5°C.

(iii) Curve marked "Expt. III" (hollow circles) shows a repetition of the previous experiment, but at temperatures displaced by 0.5°C. There is general agreement with "Expt. II."

(iv) Uppermost curve (solid and hollow circles) is a combined plot of Expt. II and III, and good concordance is obtained down to 16°C., below which there are a few substantial discrepancies. The mean graph above 16°C. has nicely regular appearance.

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Table 3.—Beckmann Reading, Flow Times and Calculated Values of E/R for Pure Benzene (Analar Grade), Using $\Delta T = 1$ °C. (Expt. III).

Heating sequence				Cooling sequence					Overall mean		
Temp. (°C.)	Beckmann reading	Time of flow (sec.) corrected for level	Mean temp. (°C.)	E'/R ÷1000	Temp. (°C.)	Beckmann reading	Time of flow (sec.) corrected for level	Mean temp. (°C.)	E'/R ÷1000	Mean (E/R)/ 1000 f	Standard deviation or group
12.0 13.0 14.0 15.0 16.0	$5.635 \pm 0.001 \\ 4.612 \pm 0.001 \\ 3.598 \pm 0.000 \\ 2.556 \pm 0.000 \\ 1.561 \pm 0.001$	$\begin{array}{c} 207.33 \pm 0.01 \\ 204.20 \pm 0.02 \\ 201.21 \pm 0.04 \\ 198.35 \pm 0.01 \\ 195.81 \pm 0.03 \end{array}$	12.50 13.50 14.50 15.50	1.213 1.195 1.137 1.079	12.0 13.0 14.0 15.0 16.0	$\begin{array}{c} 5.637 \pm 0.001 \\ 4.615 \pm 0.001 \\ 3.587 \pm 0.000 \\ 2.546 \pm 0.000 \\ 1.578 \pm 0.001 \end{array}$	$\begin{array}{c} 207.23 \pm 0.06 \\ 204.33 \pm 0.05 \\ 201.34 \pm 0.03 \\ 198.79 \pm 0.09 \\ 196.33 \pm 0.05 \end{array}$	12.50 13.50 14.50 15.50	1.133 1.178 1.013 1.072	$\begin{array}{c} 1.173 \pm 0.040 \\ 1.186 \pm 0.008 \\ 1.075 \pm 0.062 \\ 1.076 \pm 0.004 \end{array}$	0.032
16.0 17.0 18.0 19.0 20.0	$\begin{array}{c} 5.565 \pm 0.000 \\ 4.549 \pm 0.000 \\ 3.516 \pm 0.001 \\ 2.512 \pm 0.001 \\ 1.514 \pm 0.001 \end{array}$	$\begin{array}{c} 195.18 \pm 0.02 \\ 192.42 \pm 0.03 \\ 190.05 \pm 0.03 \\ 187.54 \pm 0.05 \\ 185.16 \pm 0.02 \end{array}$	16.50 17.50 18.50 19.50	1.176 1.014 1.126 1.096	16.0 17.0 18.0 19.0 20.0	$\begin{array}{c} 5.561 {\pm} 0.001 \\ 4.546 {\pm} 0.001 \\ 3.517 {\pm} 0.001 \\ 2.511 {\pm} 0.000 \\ 1.511 {\pm} 0.001 \end{array}$	$\begin{array}{c} 195.15 {\pm} 0.04 \\ 192.59 {\pm} 0.10 \\ 190.16 {\pm} 0.04 \\ 187.68 {\pm} 0.05 \\ 185.22 {\pm} 0.08 \end{array}$	16.50 17.50 18.50 19.50	1.092 1.042 1.110 1.130	$\begin{array}{c} 1.134 \pm 0.042 \\ 1.028 \pm 0.014 \\ 1.118 \pm 0.008 \\ 1.113 \pm 0.017 \end{array}$	0.024
20.0 21.0 22.0 23.0 24.0	$\begin{array}{c} 5.226 \pm 0.000 \\ 4.231 \pm 0.000 \\ 3.208 \pm 0.001 \\ 2.188 \pm 0.000 \\ 1.191 \pm 0.001 \end{array}$	$\begin{array}{c} 184.96 \pm 0.03 \\ 182.55 \pm 0.03 \\ 180.11 \pm 0.04 \\ 177.96 \pm 0.02 \\ 175.74 \pm 0.01 \end{array}$	20.50 21.50 22.50 23.50	1.136 1.142 1.030 1.106	20.0 21.0 22.0 23.0 24.0	$5.237 \pm 0.001 \\ 4.234 \pm 0.001 \\ 3.195 \pm 0.000 \\ 2.197 \pm 0.001 \\ 1.196 \pm 0.001$	$184.66 \pm 0.03 \\ 182.27 \pm 0.03 \\ 179.78 \pm 0.03 \\ 177.58 \pm 0.05 \\ 175.45 \pm 0.03 \\ 175.45 \pm 0.03 \\ 175.45 \pm 0.03 \\ 175.45 \pm 0.03 \\ 1000 \pm 0.00 $	20.50 21.50 22.50 23.50	1.120 1.149 1.078 1.061	$\begin{array}{c} 1.128 \pm 0.008 \\ 1.149 \pm 0.004 \\ 1.054 \pm 0.024 \\ 1.083 \pm 0.022 \end{array}$	0.016
24.0 25.0 26.0 27.0 28.0	$5.404 \pm 0.001 \\ 4.412 \pm 0.001 \\ 3.384 \pm 0.001 \\ 2.380 \pm 0.000 \\ 1.386 \pm 0.001 \\ \end{array}$	$\begin{array}{c} 175.14 \pm 0.03 \\ 173.00 \pm 0.03 \\ 170.81 \pm 0.04 \\ 168.68 \pm 0.62 \\ 166.69 \pm 0.04 \end{array}$	24.50 25.50 26.50 27.50	1.098 1.105 1.122 1.079	24.0 25.0 26.0 27.0 28.0	$\begin{array}{c} 5.419 \pm 0.001 \\ 4.404 \pm 0.001 \\ 3.378 \pm 0.001 \\ 2.384 \pm 0.001 \\ 1.383 \pm 0.000 \end{array}$	$\begin{array}{c} 175.32 \pm 0.02 \\ 173,15 \pm 0.02 \\ 170.98 \pm 0.00 \\ 168.82 \pm 0.04 \\ 166.68 \pm 0.04 \end{array}$	24.50 25.50 26.50 27.50	1.093 1.087 1.148 1.152	$\begin{array}{c} 1.095 \pm 0.002 \\ 1.096 \pm 0.009 \\ 1.135 \pm 0.013 \\ 1.116 \pm 0.036 \end{array}$	0.018
28.0 29.0 30.0 31.0	$\begin{array}{c} 4.621 \pm 0.001 \\ 3.614 \pm 0.001 \\ 2.592 \pm 0.001 \\ 1.609 \pm 0.001 \end{array}$	$\begin{array}{c} 166.52 \pm 0.04 \\ 164.52 \pm 0.02 \\ 162.55 \pm 0.02 \\ 160.59 \pm 0.01 \end{array}$	28.50 29.50 30.50	1.092 1.080 1.138	28.0 29.0 30.0 31.0	$\begin{array}{c} 4.628 \pm 0.001 \\ 3.618 \pm 0.001 \\ 2.575 \pm 0.001 \\ 1.616 \pm 0.001 \end{array}$	$\begin{array}{c} 165.70 \pm 0.05 \\ 163.87 \pm 0.02 \\ 162.00 \pm 0.04 \\ 160.23 \pm 0.03 \end{array}$	28.50 29.50 30.50	$1.000 \\ 1.008 \\ 1.056$	$\begin{array}{c} 1.046 \pm 0.046 \\ 1.044 \pm 0.036 \\ 1.097 \pm 0.041 \end{array}$	0.048
31.0 32.0 33.0 34.0	$\begin{array}{c} 4.065 \pm 0.002 \\ 3.037 \pm 0.000 \\ 2.023 \pm 0.000 \\ 1.041 \pm 0.002 \end{array}$	$\begin{array}{c} 160.70 \pm 0.02 \\ 158.75 \pm 0.02 \\ 156.88 \pm 0.02 \\ 155.14 \pm 0.03 \end{array}$	31.50 32.50 33.50	1.102 1.092 1.068	31.0 32.0 33.0 34.0	$\begin{array}{c} 4.076 \pm 0.000 \\ 3.035 \pm 0.002 \\ 2.056 \pm 0.001 \\ 1.040 \pm 0.001 \end{array}$	$\begin{array}{c} 160.76 \pm 0.02 \\ 158.85 \pm 0.00 \\ 156.95 \pm 0.01 \\ 155.07 \pm 0.02 \end{array}$	31.50 32.50 33.50	1.065 1.148 1.115	${}^{1.084 \pm 0.019}_{1.120 \pm 0.028}_{1.092 \pm 0.023}$	0.028
34.0 35.0 36.0 37.0 38.0	$\begin{array}{c} 5.137 \pm 0.001 \\ 4.150 \pm 0.001 \\ 3.137 \pm 0.000 \\ 2.127 \pm 0.000 \\ 1.132 \pm 0.002 \end{array}$	$\begin{array}{c} 154.79 \pm 0.00 \\ 153.23 \pm 0.01 \\ 151.53 \pm 0.01 \\ 149.85 \pm 0.02 \\ 148.12 \pm 0.03 \end{array}$	34.50 35.50 36.50 37.50	0.978 1.043 1.058 1.144	34.0 35.0 36.0 37.0 38.0	$\begin{array}{c} 5.162 \pm 0.001 \\ 4.161 \pm 0.001 \\ 3.128 \pm 0.001 \\ 2.126 \pm 0.001 \\ 1.128 \pm 0.001 \end{array}$	$\begin{array}{c} 155.34{\pm}0.02\\ 153.60{\pm}0.02\\ 151.73{\pm}0.02\\ 149.97{\pm}0.03\\ 148.31{\pm}0.01 \end{array}$	34.50 35.50 36.50 37.50	1.065 1.129 1.116 1.076	$\begin{array}{c} 1.022 \pm 0.042 \\ 1.086 \pm 0.043 \\ 1.087 \pm 0.019 \\ 1.110 \pm 0.034 \end{array}$	0.040
38.0 39.0 40.0 41.0 42.0	$5.463 \pm 0.002 \\ 4.465 \pm 0.001 \\ 3.470 \pm 0.002 \\ 2.460 \pm 0.001 \\ 1.465 \pm 0.002 \\ \end{array}$	$\begin{array}{c} 148.20 \pm 0.02 \\ 146.66 \pm 0.01 \\ 145.09 \pm 0.00 \\ 143.48 \pm 0.02 \\ 141.93 \pm 0.01 \end{array}$	38.50 39.50 40.50 41.50	1.017 1.057 1.087 1.080	38.0 39.0 40.0 41.0 42.0	$5.464 \pm 0.002 \\ 4.462 \pm 0.002 \\ 3.459 \pm 0.002 \\ 2.450 \pm 0.002 \\ 1.466 \pm 0.002 \\ \end{array}$	$\begin{array}{c} 148.45 \pm 0.02 \\ 146.75 \pm 0.00 \\ 145.15 \pm 0.02 \\ 143.45 \pm 0.02 \\ 141.98 \pm 0.02 \end{array}$	38.50 39.50 40.50 41.50	1.116 1.068 1.148 1.036	$\begin{array}{c} 1.066 \pm 0.050 \\ 1.062 \pm 0.006 \\ 1.118 \pm 0.030 \\ 1.058 \pm 0.022 \end{array}$	0.032
42.0 43.0 44.0 45.0 46.0	$5.429 \pm 0.002 \\ 4.416 \pm 0.002 \\ 3.415 \pm 0.001 \\ 2.404 \pm 0.002 \\ 1.408 \pm 0.001 \\ \end{array}$	$\begin{array}{c} 141.96 \pm 0.01 \\ 140.47 \pm 0.01 \\ 139.01 \pm 0.02 \\ 137.45 \pm 0.03 \\ 136.04 \pm 0.02 \end{array}$	42.50 43.50 44.50 45.50	1.038 1.046 1.126 1.051	42.0 43.0 44.0 45.0 46.0	5.410 ± 0.001 4.408 ± 0.002 3.409 ± 0.001 2.401 ± 0.001 1.404 ± 0.002	$\begin{array}{c} 141.88 \pm 0.01 \\ 140.41 \pm 0.02 \\ 138.87 \pm 0.01 \\ 137.31 \pm 0.00 \\ 135.90 \pm 0.01 \end{array}$	42.50 43.50 44.50 45.50	1.036 1.106 1.113 1.051	$\begin{array}{c} 1.037 \pm 0.001 \\ 1.073 \pm 0.027 \\ 1.120 \pm 0.007 \\ 1.051 \pm 0.000 \end{array}$	0.010

the heating and cooling sequences, together with the overall mean values. The final standard deviations are again estimated on the basis of the differences between the two sets of values.

TABLE 2.—CALCULATED VALUES OF E'/R \div 1000 =-T² ($\Delta \ln \nu / \Delta T$)/1000 for Pure Benzene, $\Delta T = 1^{\circ}$ C.

	(E'/R)/1000							
Mean temp. (°C.)	Heating sequence	Cooling sequence	Mean	Standard deviation				
8.00	1 154	1 234	1 194 1 0 040					
9.00	1.154	1.234	1.194 ± 0.040					
10.00	1.150	1.210	1.103 ± 0.033	10.000				
11.00	1 108	1.199	1.220 ± 0.020 1 201 + 0.003	± 0.028				
12.00	1.170	1 1 1 9 5	1.201 ± 0.003 1 163 ± 0.027					
12.00	1.141	1.175	1.105±0.027					
13.00	1,185	1.162	1.174 ± 0.012					
14.00	1.148	1.152	1.150 ± 0.002					
15.00	1.154	1.166	1.160 ± 0.006	+0.012				
16.00	1.180	1.160	1.170 ± 0.010	T 0.012				
17.00	1.148	1.080	1.114 ± 0.034					
			(100)					
18.00	1.184	1.040	1.112 ± 0.072					
19.00	1.164	1.168	1.166 ± 0.002					
20.00	1.066	1.181	1.123 ± 0.058	+0.040				
21.00	1.080	1.134	1.107 ± 0.027	an The Art of the				
22.00	1.085	1.113	1.099 ± 0.014					
	1.010	1 0 7 1						
23.00	1.219	1.076	1.148 ± 0.072					
24.00	1.100	1.081	1.090 ± 0.010	10000				
25.00	1.070	1.078	$1.0/4 \pm 0.004$	± 0.026				
26.00	1.113	1.106	1.109 ± 0.003					
27.00	1.098	1.134	1.116 ± 0.018					
28.00	1.100	1.116	1 108 + 0 008					
29.00	1.102	1.000	1.051 ± 0.051					
30.00	1.108	0.976	1.042 ± 0.066	+0.033				
31.00	1.109	1.078	1.093 ± 0.015	T 01000				
32.00	1.096	1.106	1.101 ± 0.005					
33.00	1.080	1.132	1.106 ± 0.026					
34.00	1.023	1.090	1.056 ± 0.034					
35.00	1.010	1.092	1.051 ± 0.041	± 0.030				
36.00	1.032	1.049	1.040 ± 0.009					
37.00	1.052	1.096	$1.0/4 \pm 0.022$					
38.00	1 113	1 096	1 104 - 0 008					
39.00	1.037	1.089	1.063 ± 0.026					
40.00	1.072	1.108	1.090 ± 0.018	+0.025				
41.00	1.083	1.092	1.087 ± 0.005	1 0.025				
42.00	1.059	0.948	1.004 ± 0.055					
12.00	1.042	0.002	1 012 1 0 020					
43.00	1.042	0.983	1.013 ± 0.030	10.020				
44.00	1.080	1.109	1.098 ± 0.011	± 0.030				
45.00	1.092	1.014	1.055±0.039					

Overall standard deviation = \pm 0.030

These over-all mean values are plotted as hollow circles in the upper half of Fig. 1, the graph being labelled Expt. III.

4. Conclusions

The graphs for Expts. II and III show a satisfactory measure of correspondence in the positions of the maxima and minima, and therefore a combined plot is shown in the top-most graph of Fig. 1, the data from the two experiments being plotted with solid and hollow circles as before. This combined plot is a considerable improvement on the individual graphs and enables us to draw a nicely undulating regular graph down to a temperature of 16°C. or so, with the individual points showing an r.m.s. scatter about the graph of only \pm 0.022, which compares with the estimated standard deviations ranging from 0.02 to 0.04 in Tables 2 and 3. It follows that the deviation for the mean of pairs of successive points (from Expts. II and III) 0.5° apart is \pm 0.016, while the peak-to-peak amplitude of the undulations in this graph lies between 0.06 and 0.10, i.e. four to six times this standard deviation for the means of successive points. Below 16°C., there are some large discrepancies between the results for Expt. II and Expt. III, which could be due to the presence of traces of water in the benzene, which became slightly milky below 12°C., corresponding to about 0.03% water content.

Thus we may conclude the existence of a definite, more or less cyclic, variation in activation energy E_{η} for flow of benzene in the range of 16 °C. to 46°C., the period being nearly 4.0° ± 0.9 °C. and the amplitude about 8% of the mean value. Further experiments are being carried out on heptane, on benzene of various degrees of purity, and on light mineral oils, such as high-speed diesel oil.

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